

# Frequency Selective Surface-Based Sensing for Concurrent Temperature and Strain Measurement: Benefits, Challenges, and Applications

---

Mahboobeh Mahmoodi and Kristen M. Donnell

Microwave Sensing ( $\mu$ Sense) Laboratory

Electrical and Computer Engineering

301 W 16<sup>th</sup> St

Missouri University of Science and Technology

Rolla, MO 65409, USA

kmdgfd@mst.edu

Doyle T. Motes, P.E.

Texas Research Institute (TRI) Austin, Inc.

9063 Bee Caves Rd.

Austin, TX 78733 (USA)

- Introduction to Frequency Selective Surfaces (FSSs) and FSS-based sensing
- Similar technologies
- FSS-based sensor designs
  - Concurrent temperature and strain sensing
- Practical challenges and solutions
  - Sensor resolution and key parameters
  - Sensor cell analysis and localized sensing
  - Performance improvement by FSS miniaturization
- Concluding remarks

# What is a Frequency Selective Surface?

Sample Elements



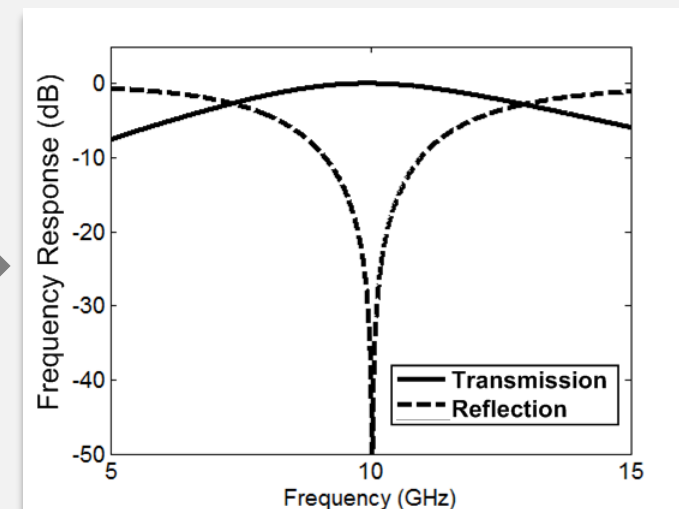
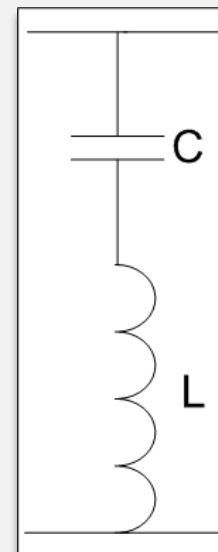
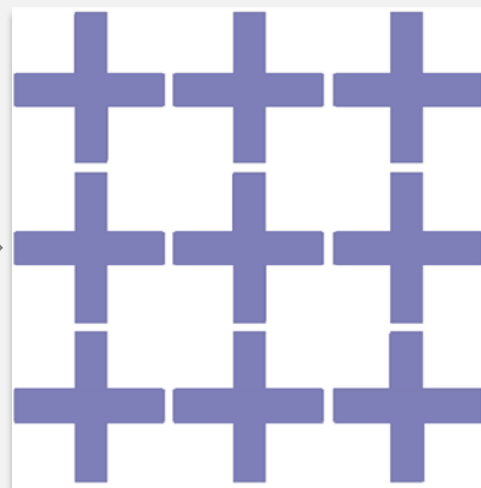
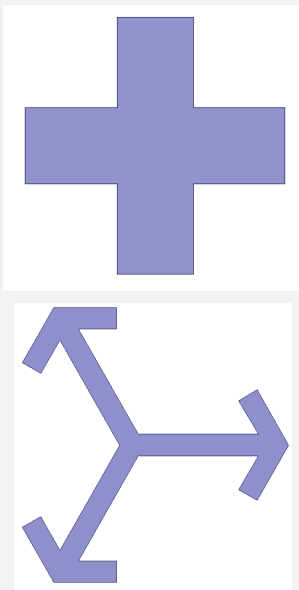
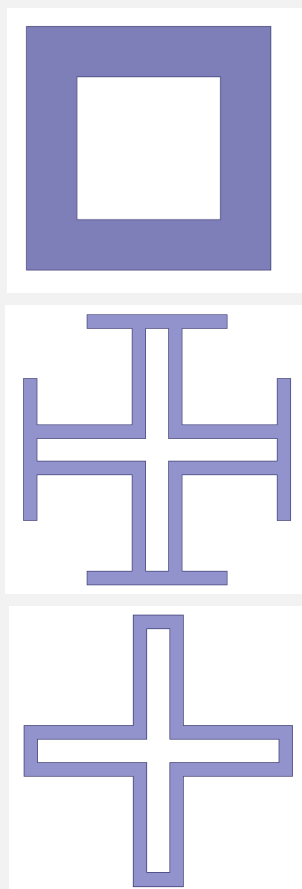
Array



Model



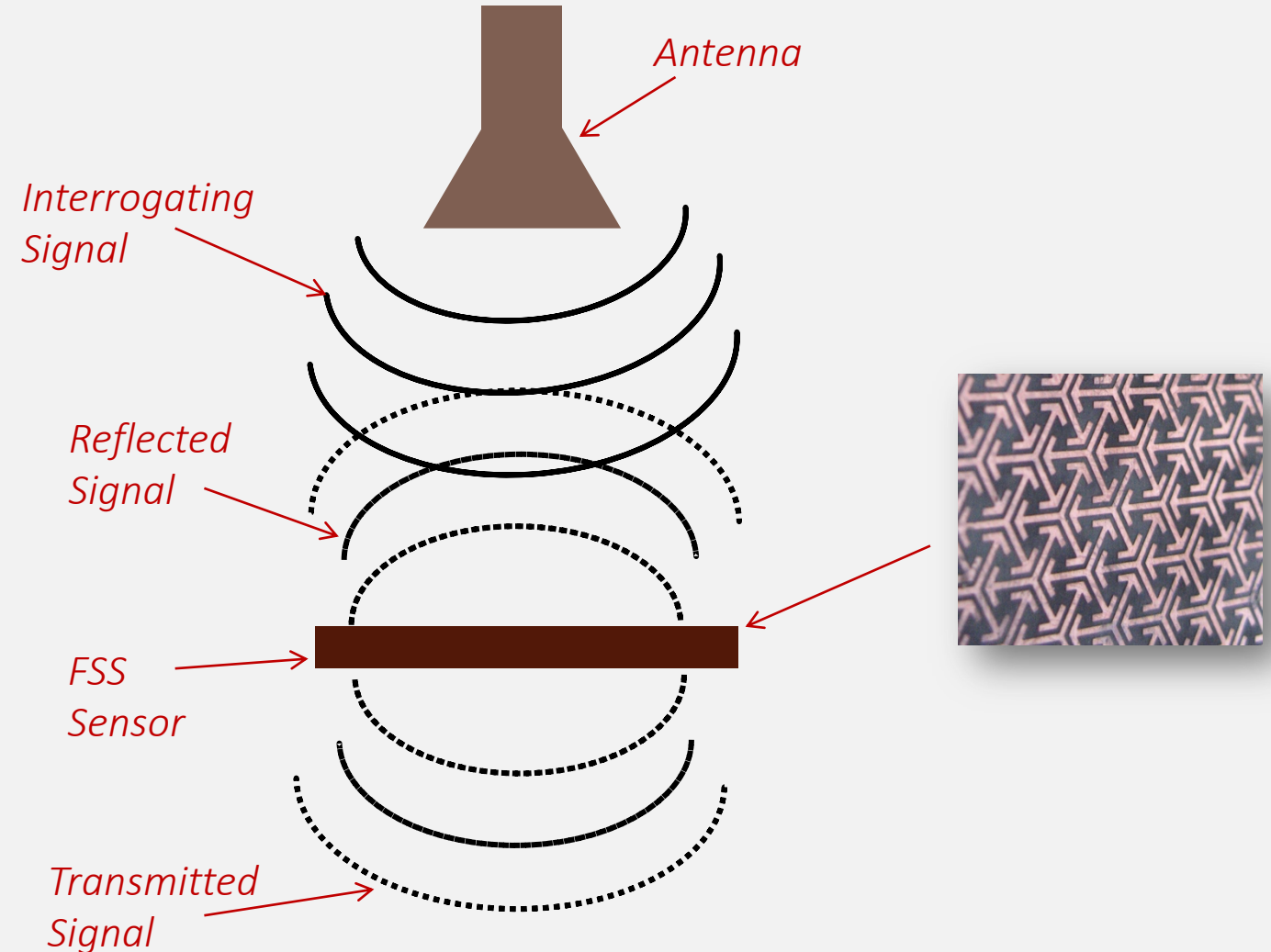
Frequency Response



# Why FSS-Based Sensing?

## ■ FSS Sensor Advantages:

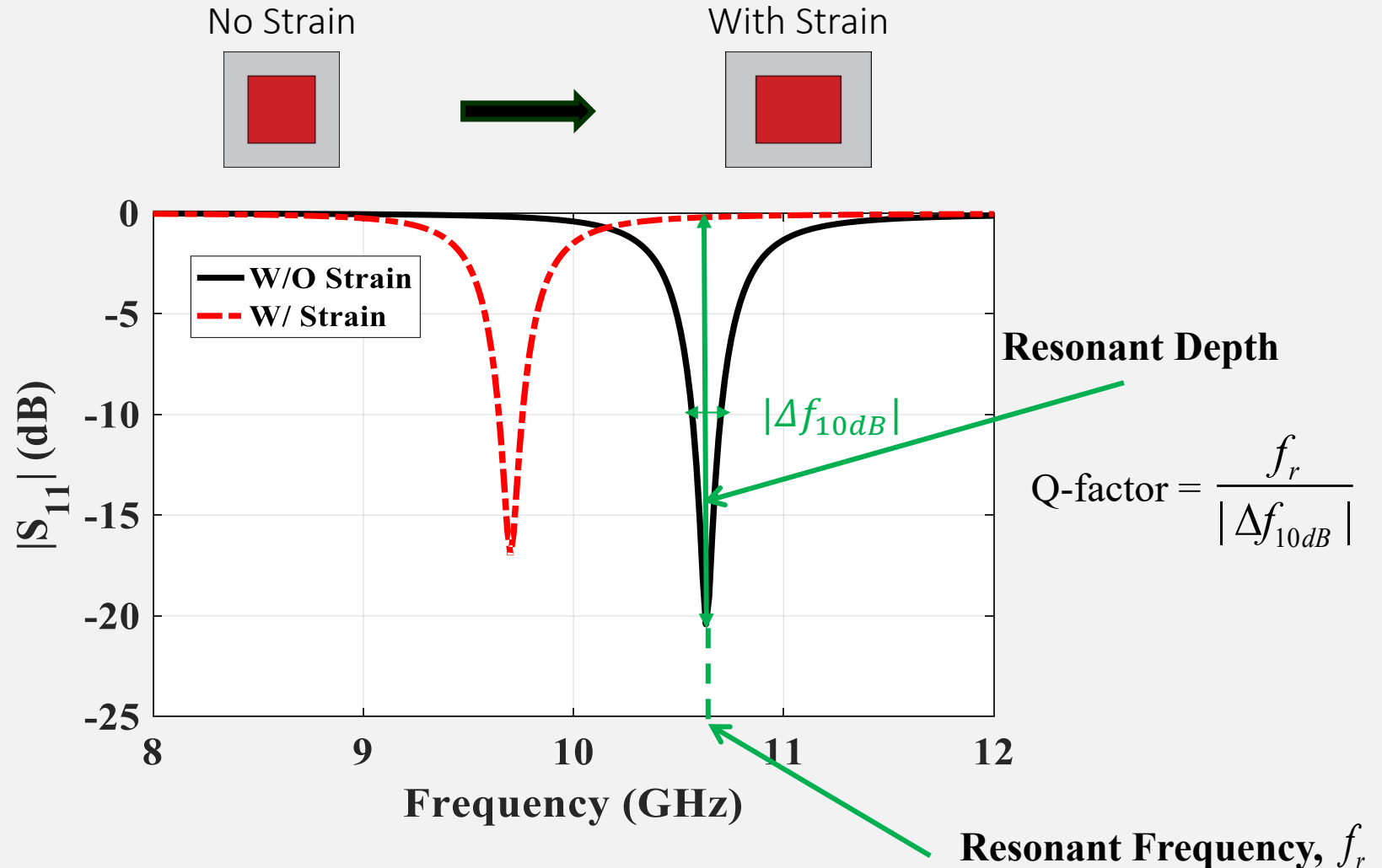
- Passive sensing
- Wireless (remote) interrogation
- Sensitive to geometrical and physical parameters
- Distributed sensing
- Extreme design flexibility – the sky is the limit!!





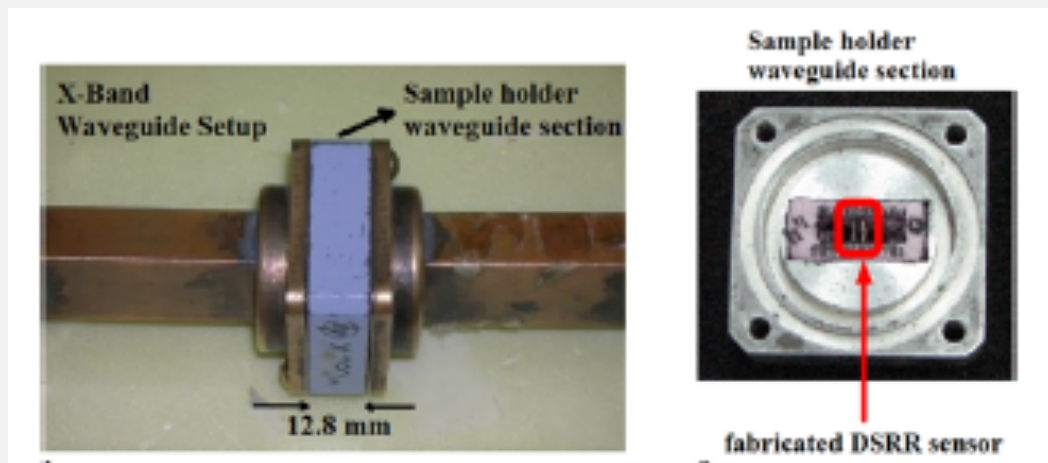
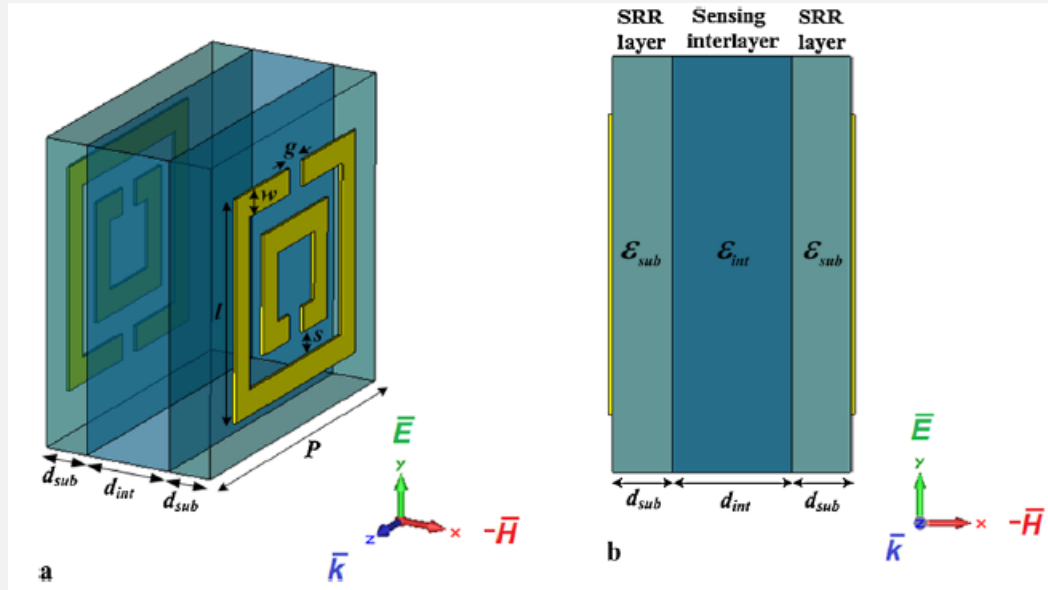
# Example FSS Sensing Applications

- 1D/2D strain
- Temperature
- Pressure
- Layered structure evaluation
- Moisture detection
- Multi-functional sensing (i.e. concurrent temperature and strain)
- Etc.....



# Why Microwave Frequencies?

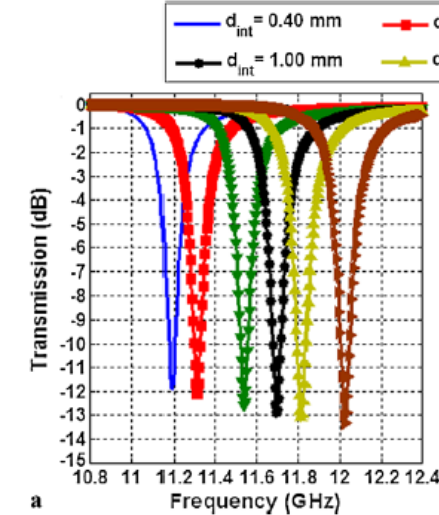
- Microwave/millimeter wave components are commercially available and low-cost
- Interrogation systems are safe, low power, and easy to use
- Antenna size is inversely proportional to frequency.
  - Becomes prohibitive, along with the FSS element/unit cell size, for lower frequencies
  - Limits the resolution (all related to wavelength)
- Resolution can be improved with increasing frequency
  - Eventually (beyond mm-wave), increasing system cost/complexity is of concern (i.e, THz, optics/laser....)



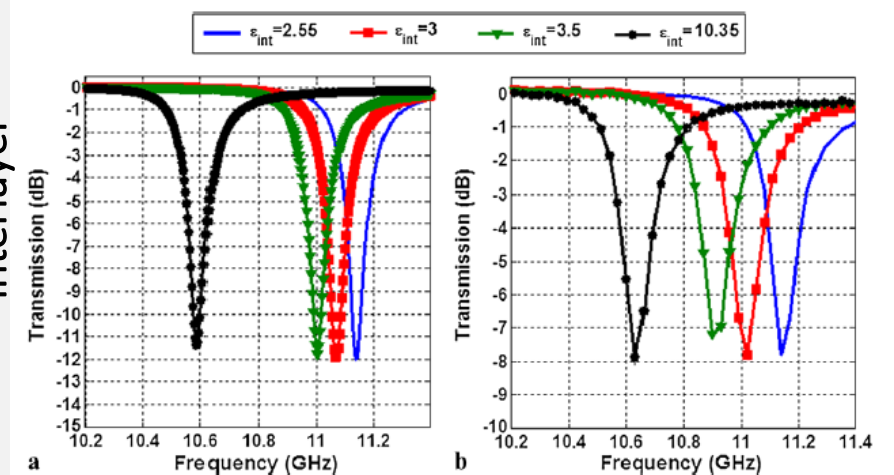
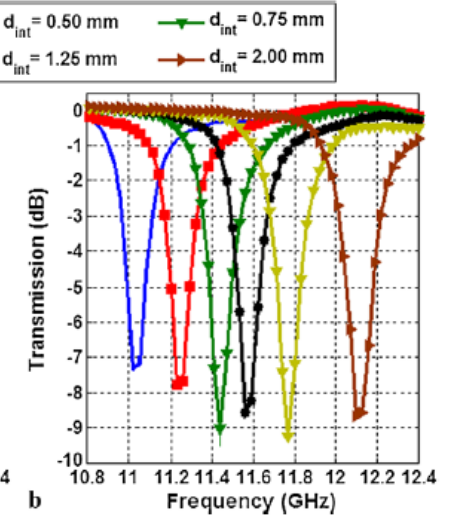
Sensitivity to thickness  
of sensing interlayer

Sensitivity to  
permittivity of sensing  
interlayer

## Simulation

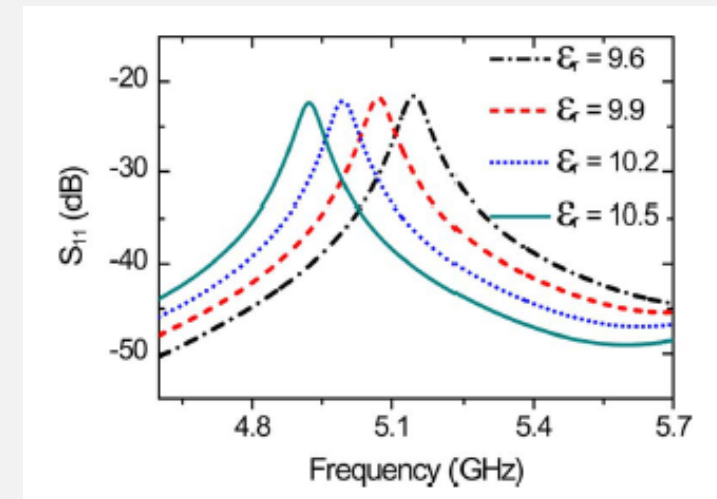
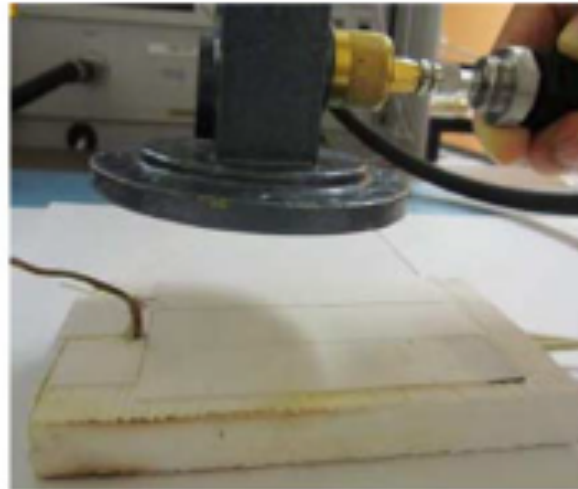
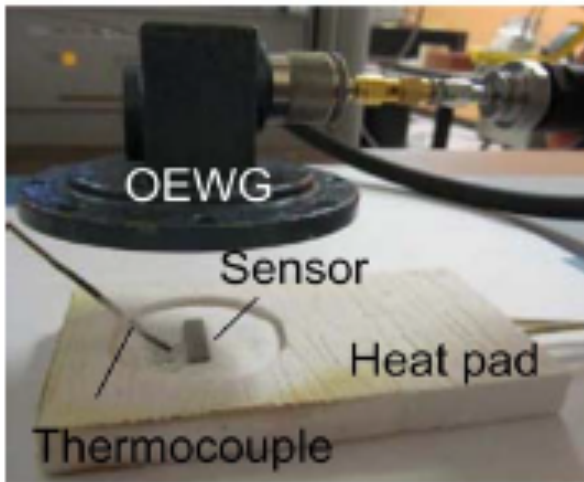
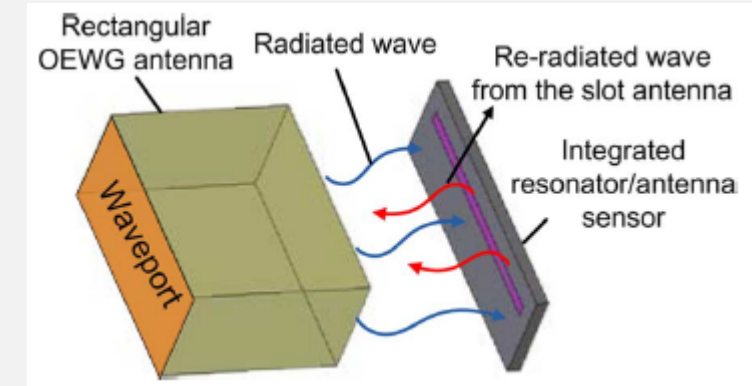


## Measurement



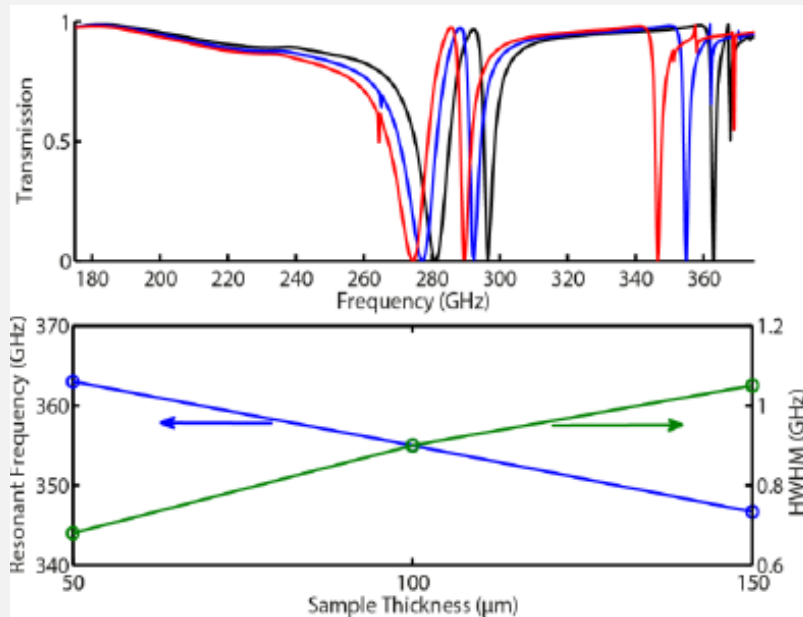
# Temperature Sensor by Resonator Integration

- Substrate is a temperature-dependent dielectric material.
- Resonant frequency of the sensor decreases from 5.12 GHz to 4.74 GHz for 50 °C to 1000 °C.
- This corresponds to a relative permittivity of 9.7 to 11.2 for the alumina substrate.

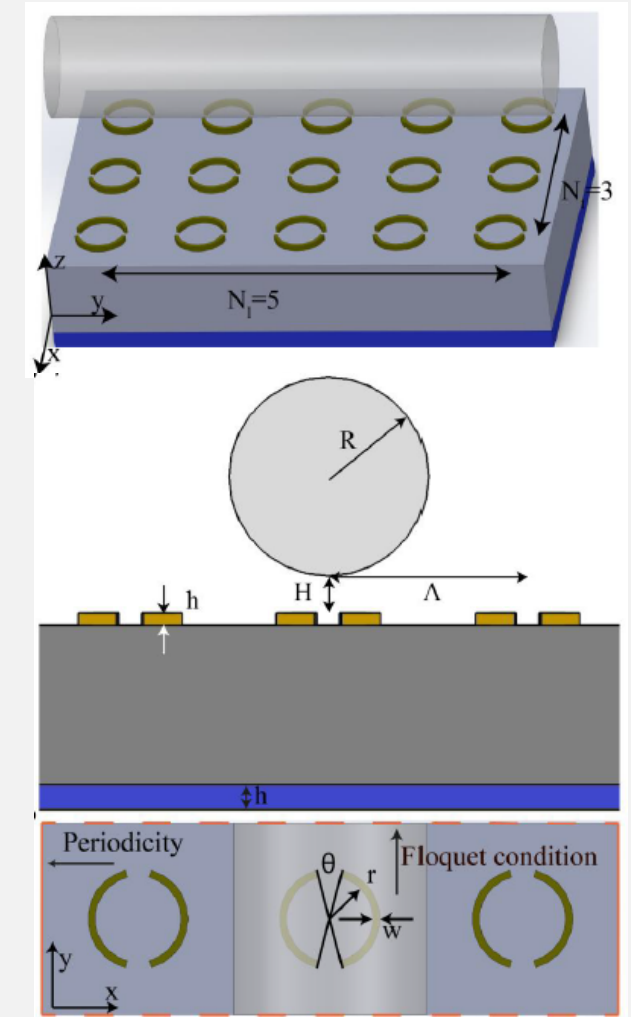
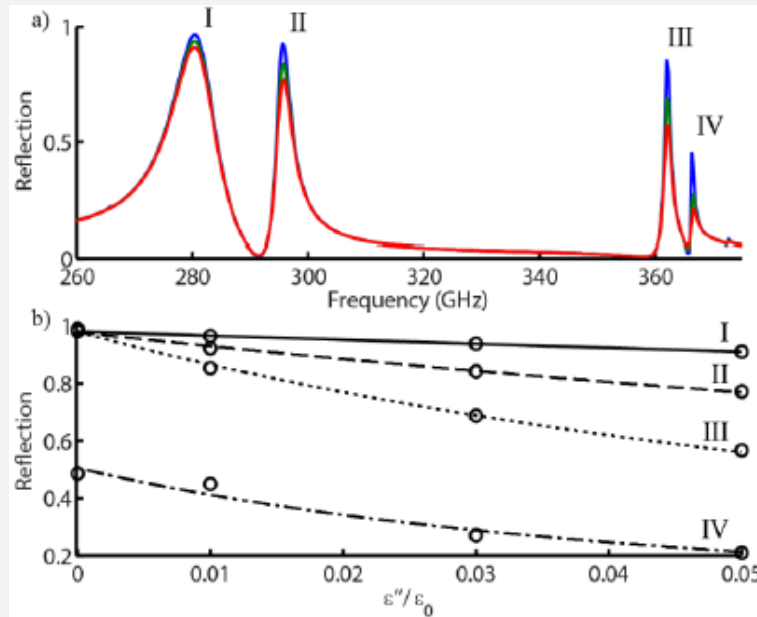


- Biomedical and chemical applications
- THz FSSs interrogated with THz subwavelength optical fibers
  - Used for monitoring optical properties of thick films

Film Thickness Sensing

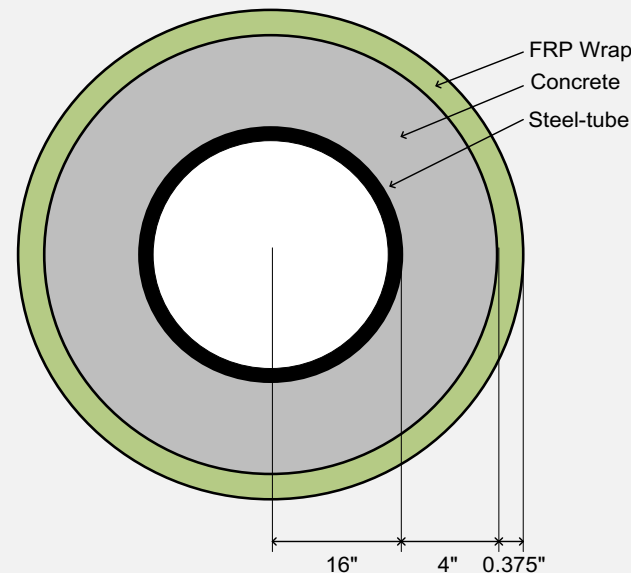


Humidity Content Sensing



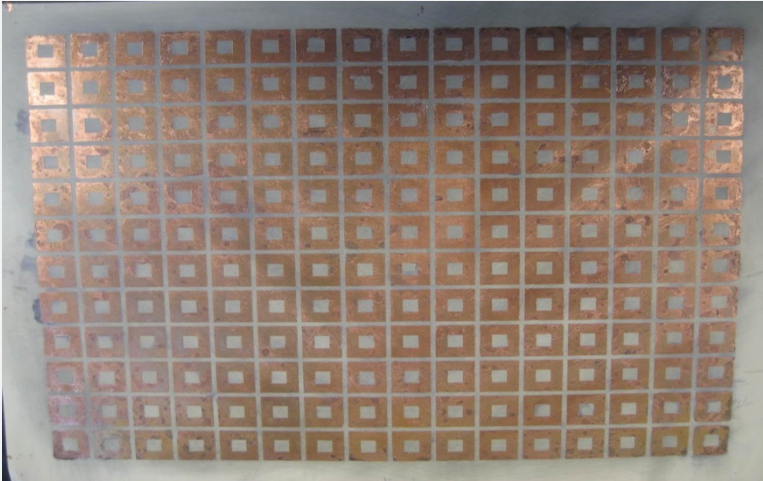


- Concrete column formed around a hollow steel core.
  - Structural stability is comparable to traditional solid concrete columns, but with reduced weight.
- Additionally, a fiber-reinforced polymer (FRP) layer surrounds the concrete.
  - Serves as a casing during casting and provides protection from the environment.



# FSS for SHM – Curved Surfaces

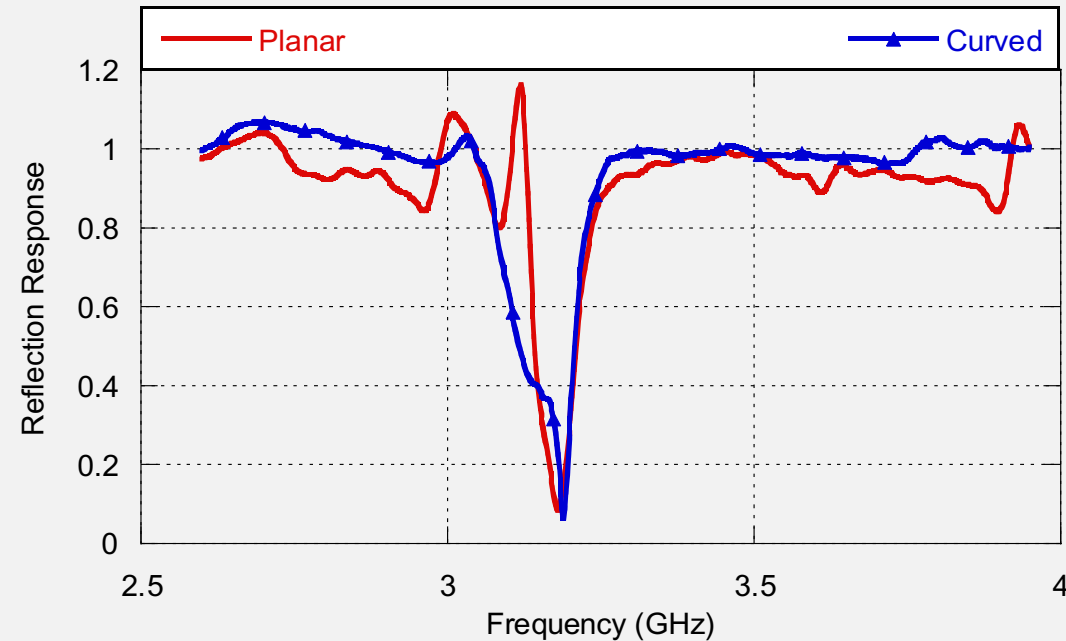
*FSS Sensor*



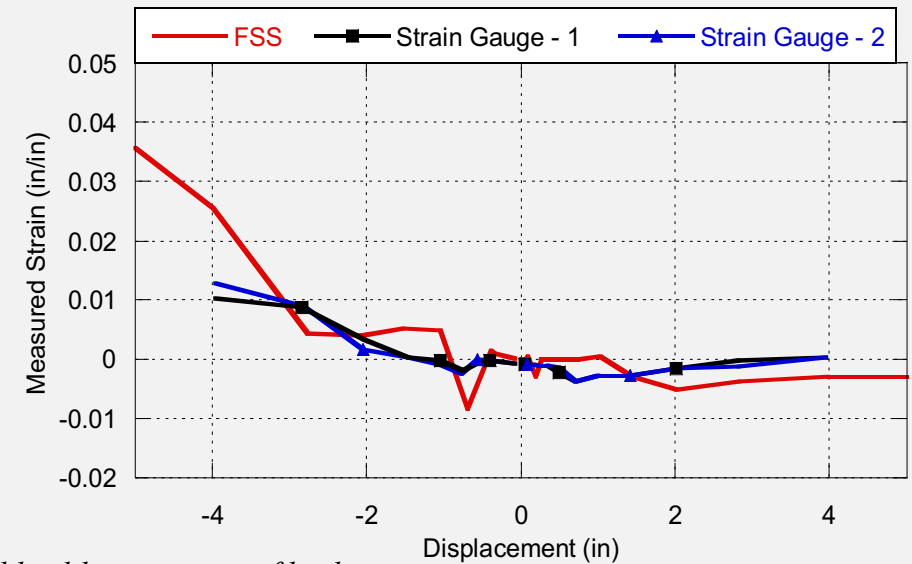
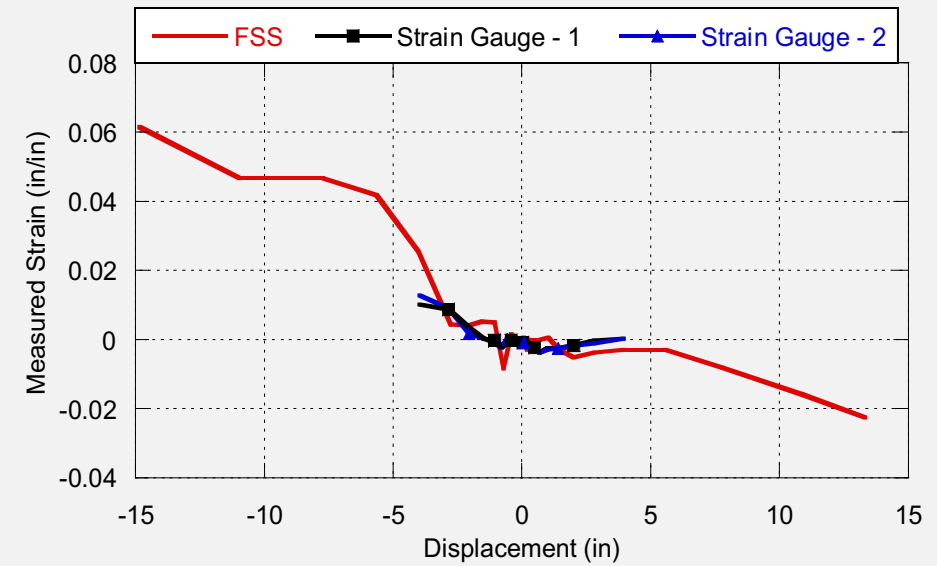
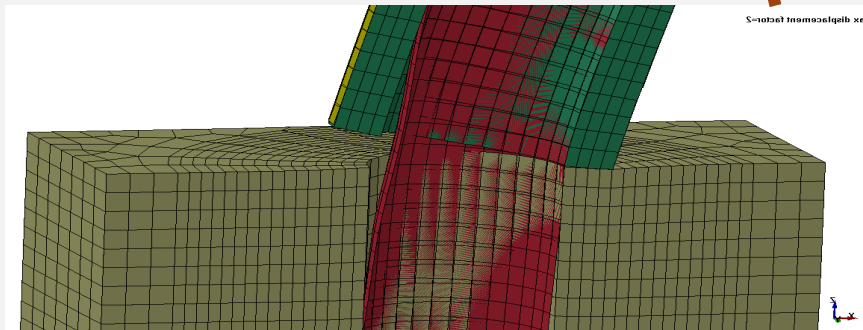
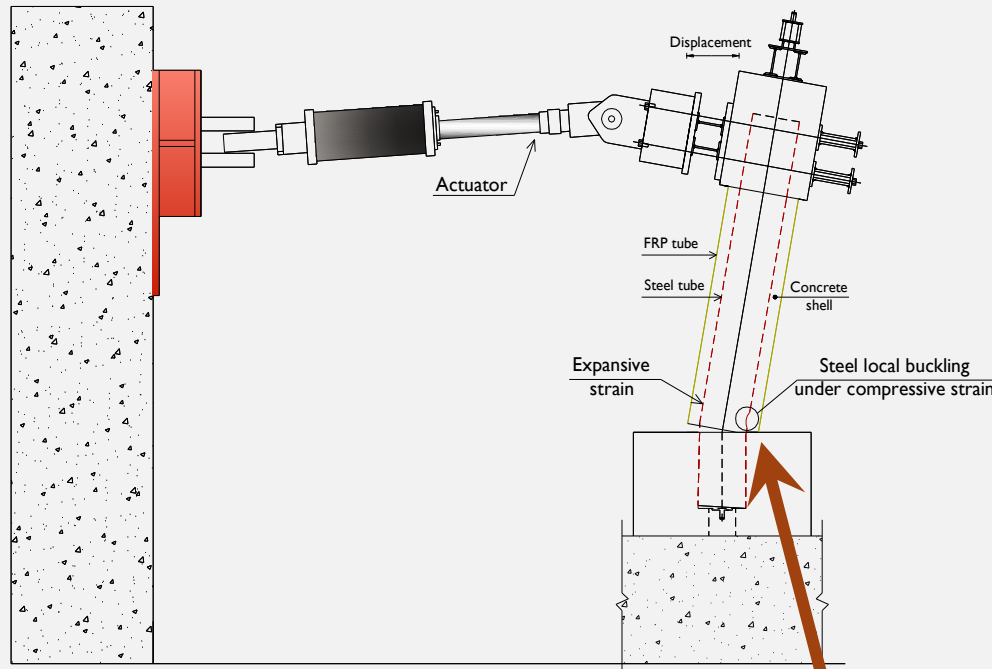
*Sensor Placement*



*3D Printed Horn Antenna*



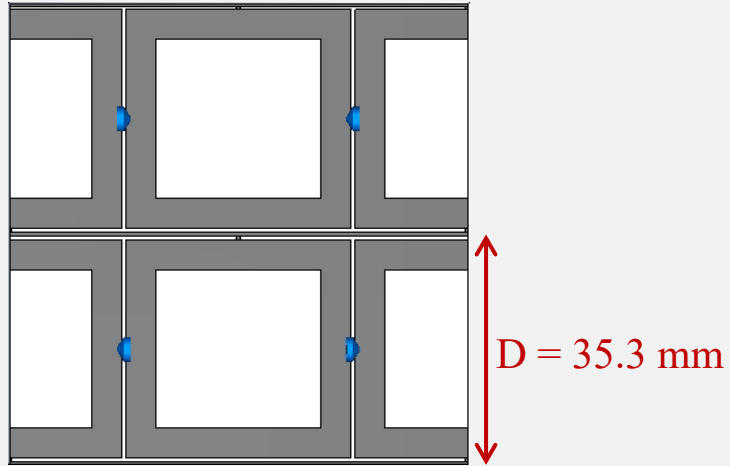
# FSS for SHM



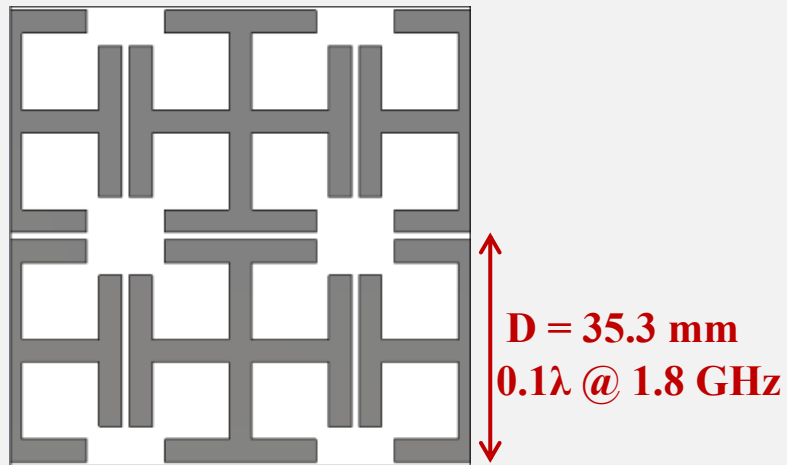


# Active FSS for Strain Sensing

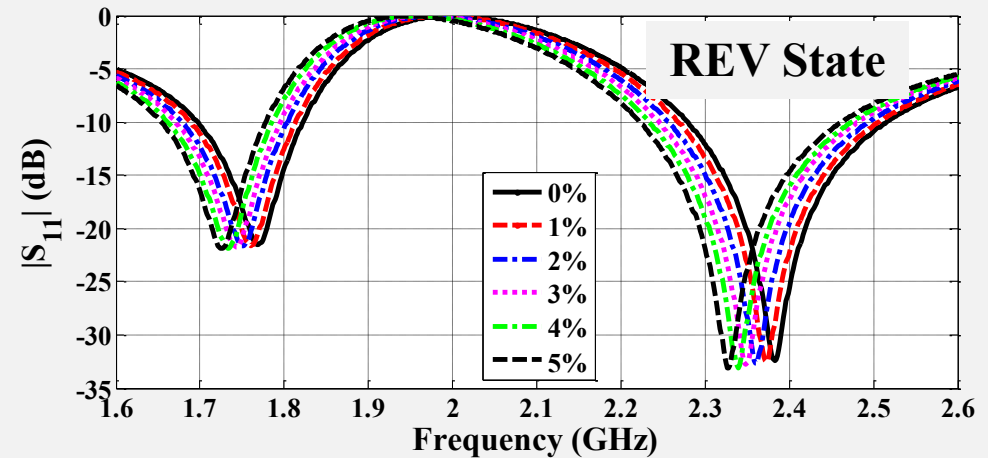
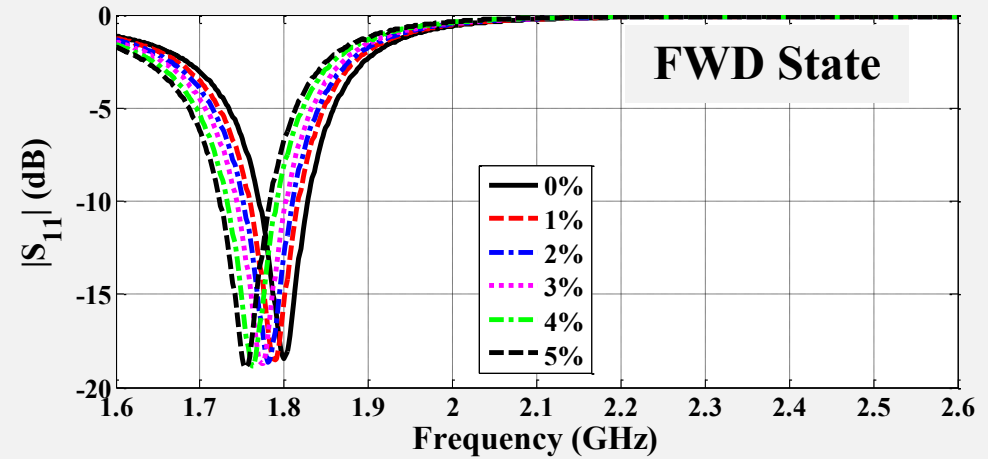
Active FSS  
(Bottom Layer)



Passive FSS  
(Top Layer)

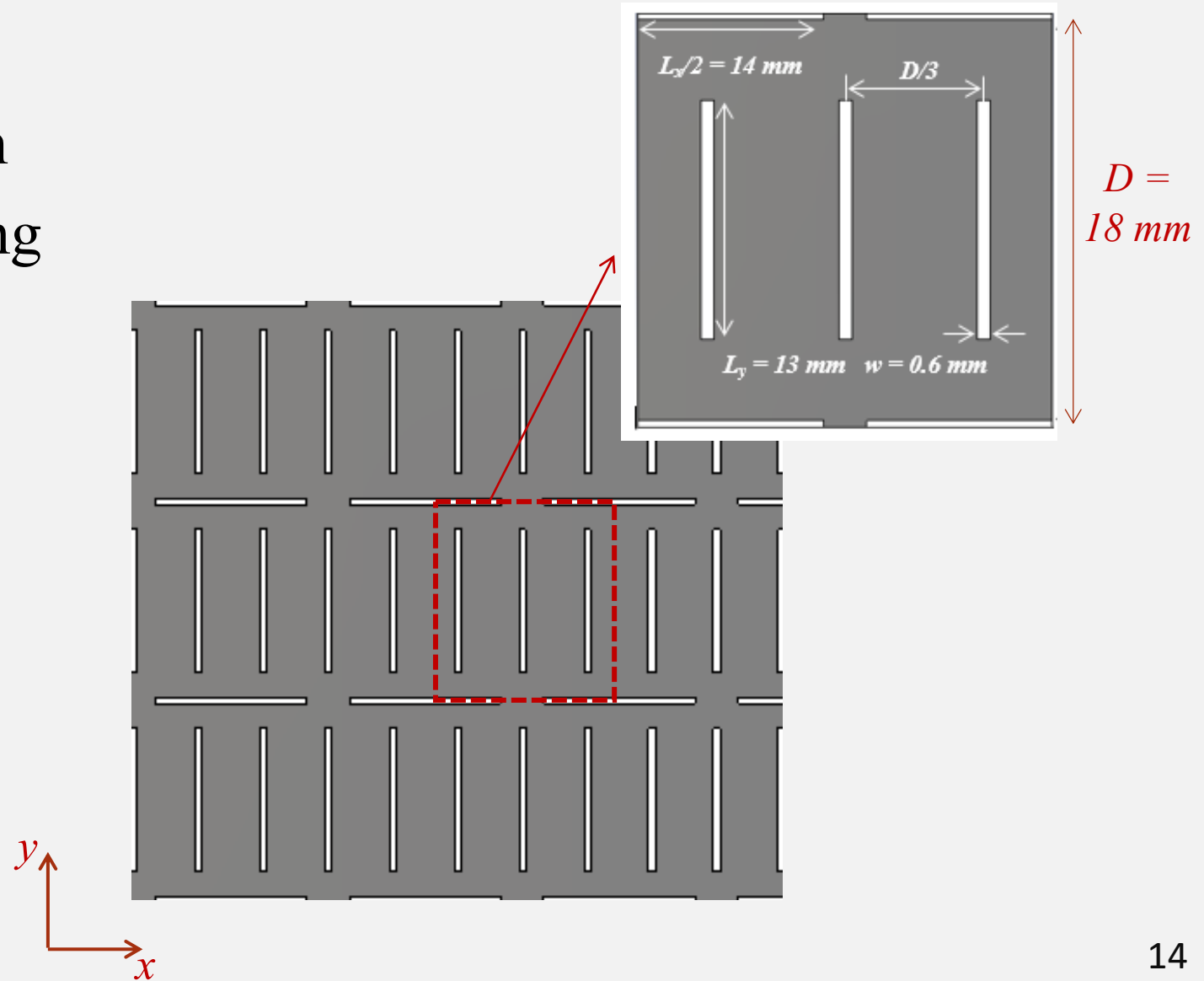


Substrate: Rogers 5880, 20 mils,  $\epsilon_r = 2.2$ ,  $\tan\delta = 0.0009$



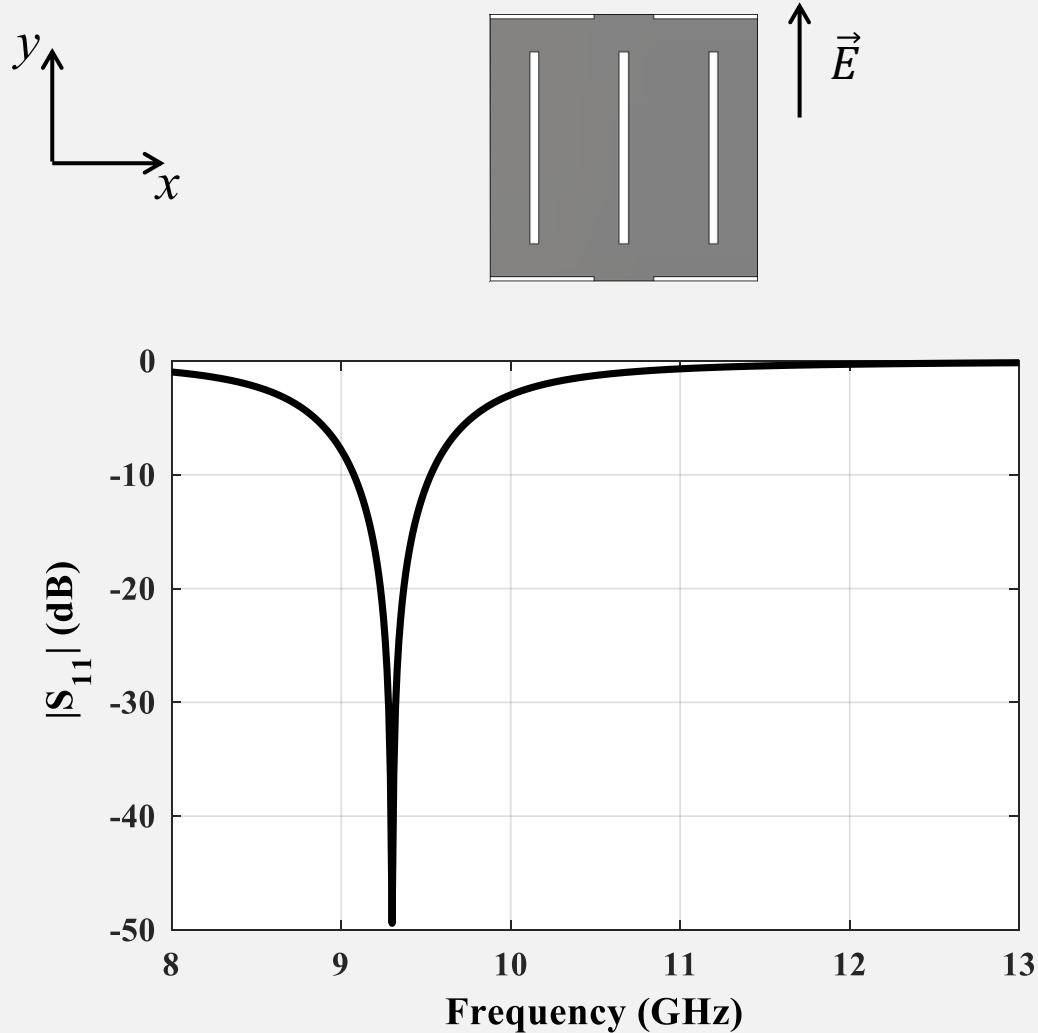
# 2D In-Plane Normal Strain Sensor

- Flexibility to monitor 2D strain using dual-polarized FSS design
- Provide reflection response using a slot-based element
- Strain in each direction can be characterized by measuring the reflection response polarized perpendicular to the strain direction

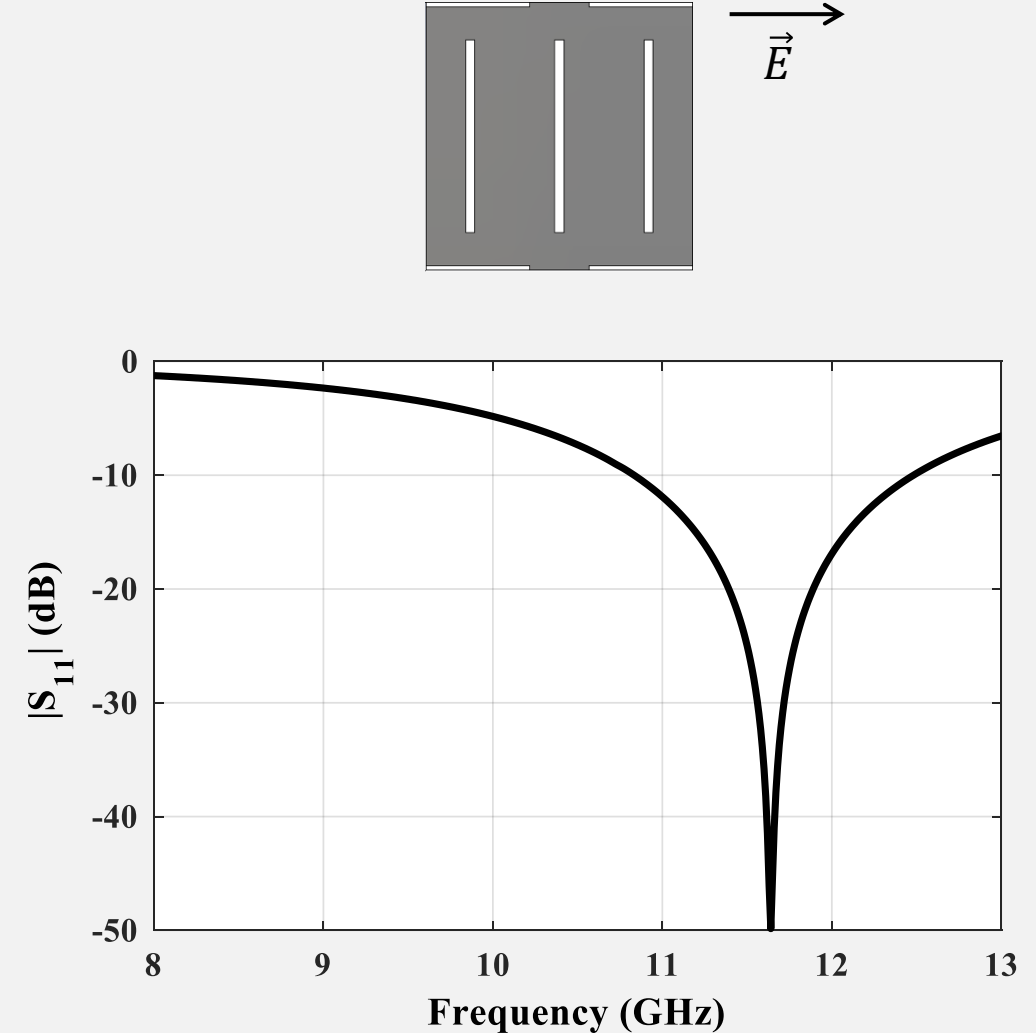


# Frequency Response of the Sensor

**Y-Pol**

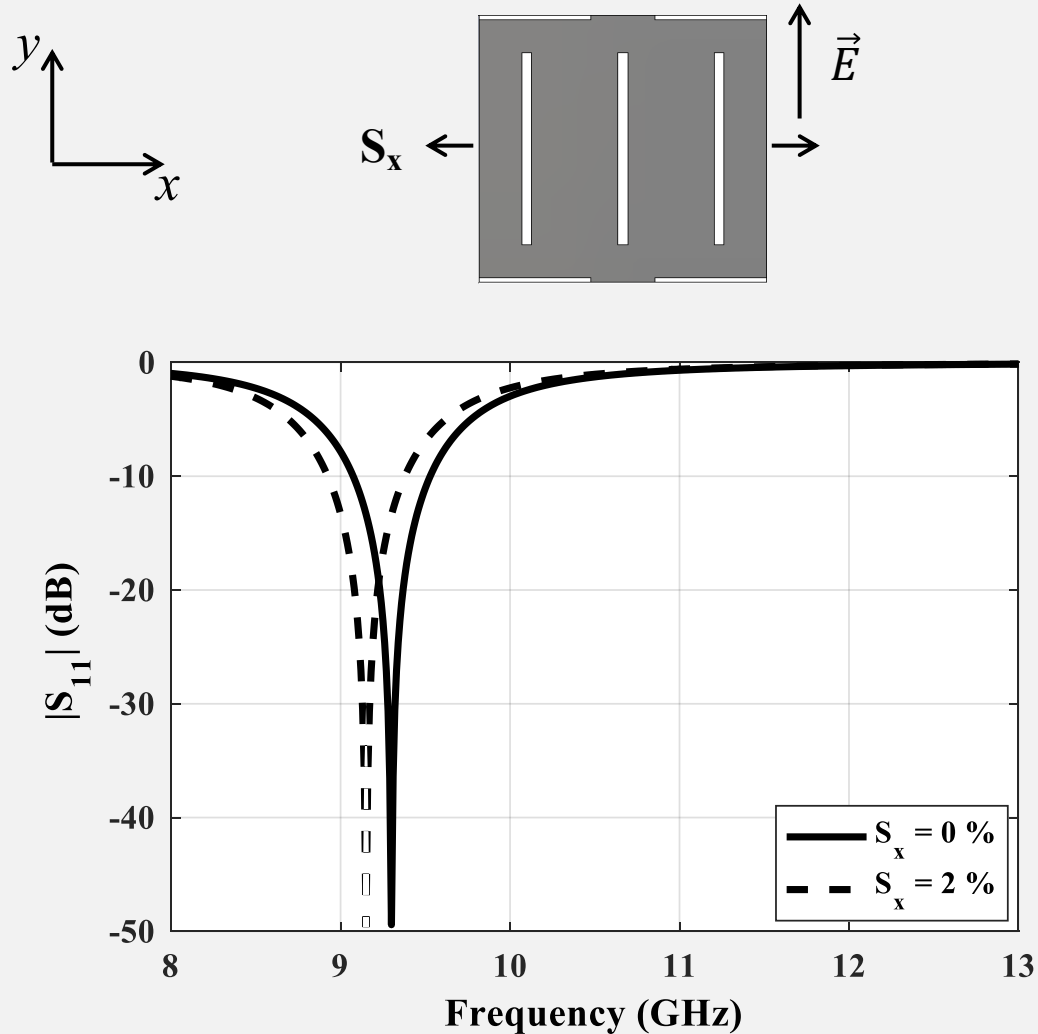


**X-Pol**

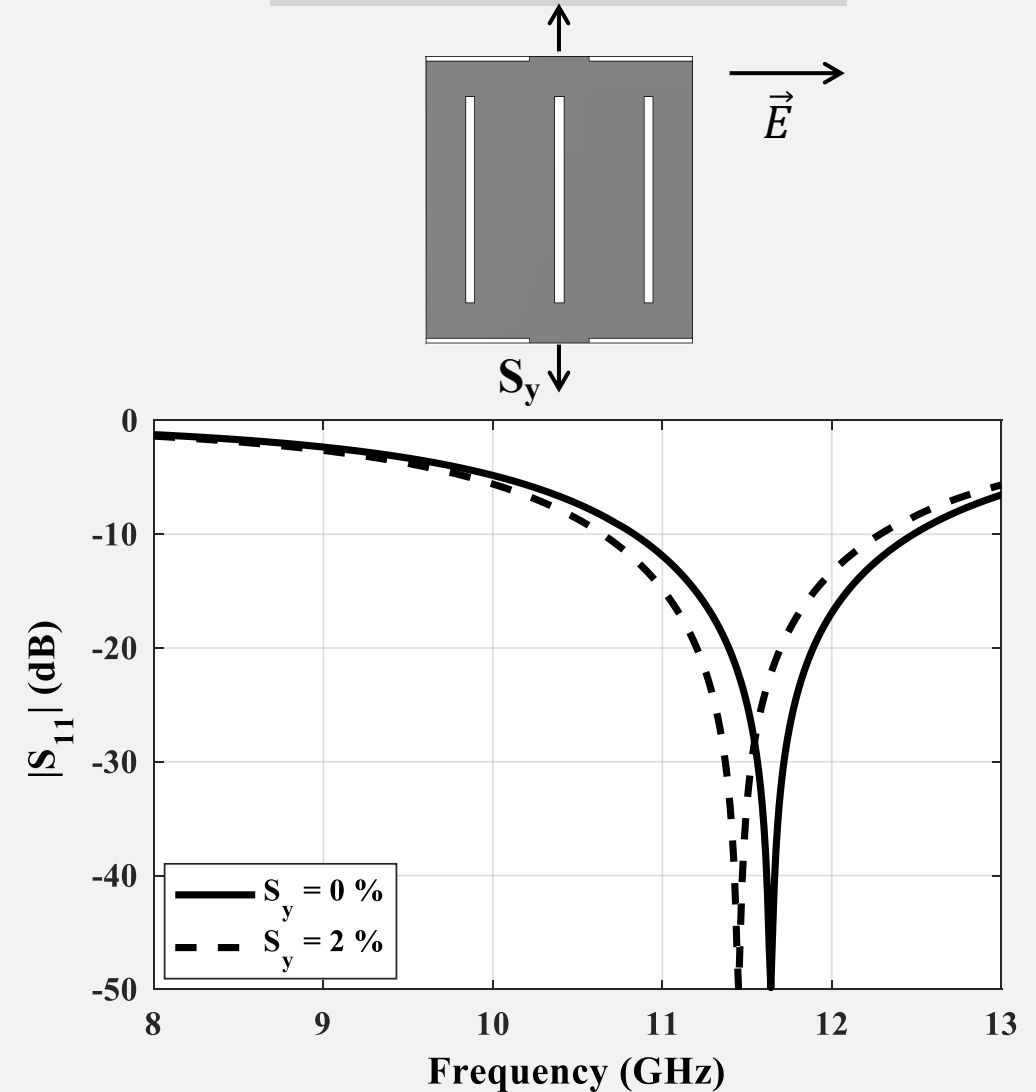


# Frequency Response of the Sensor

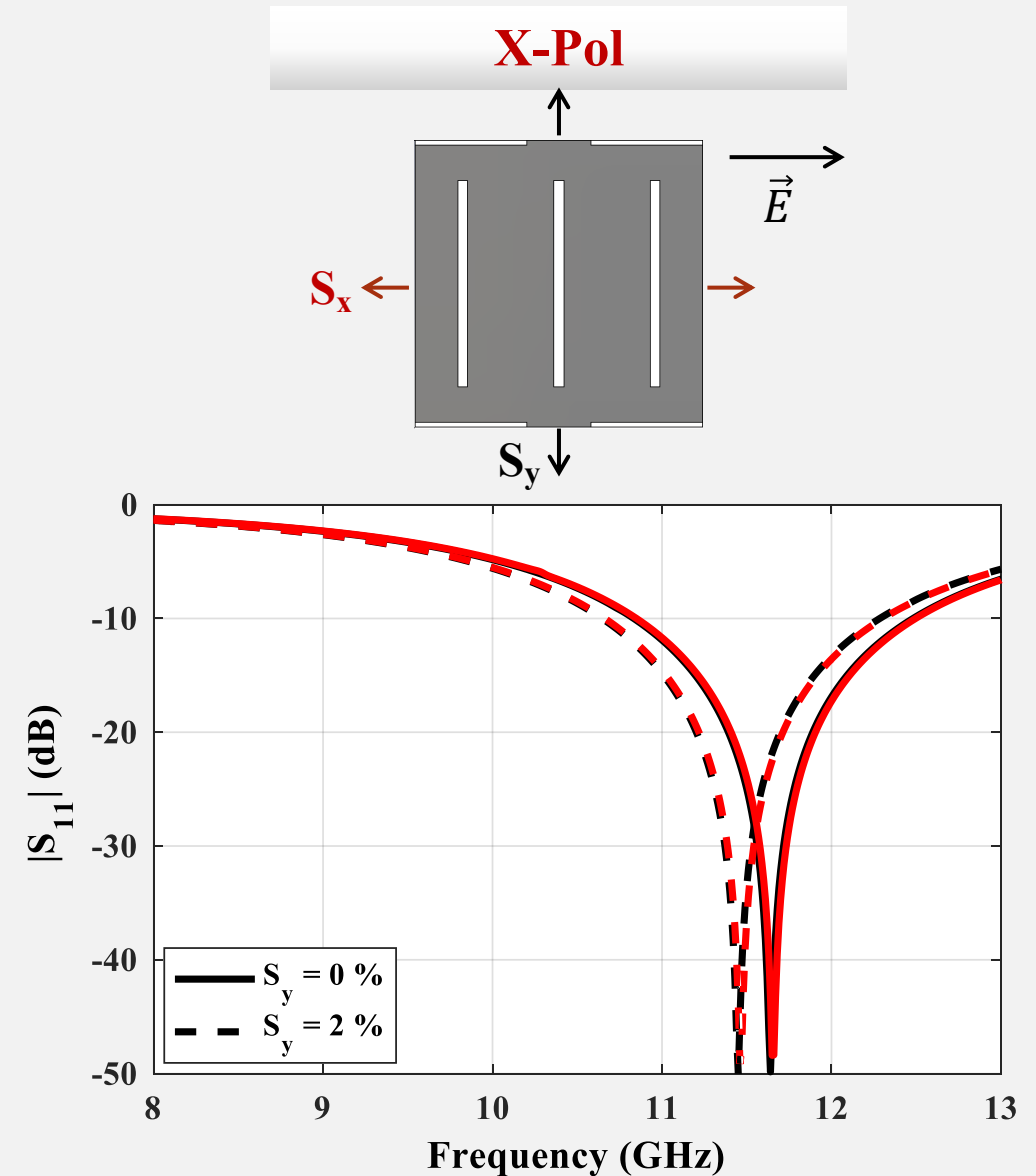
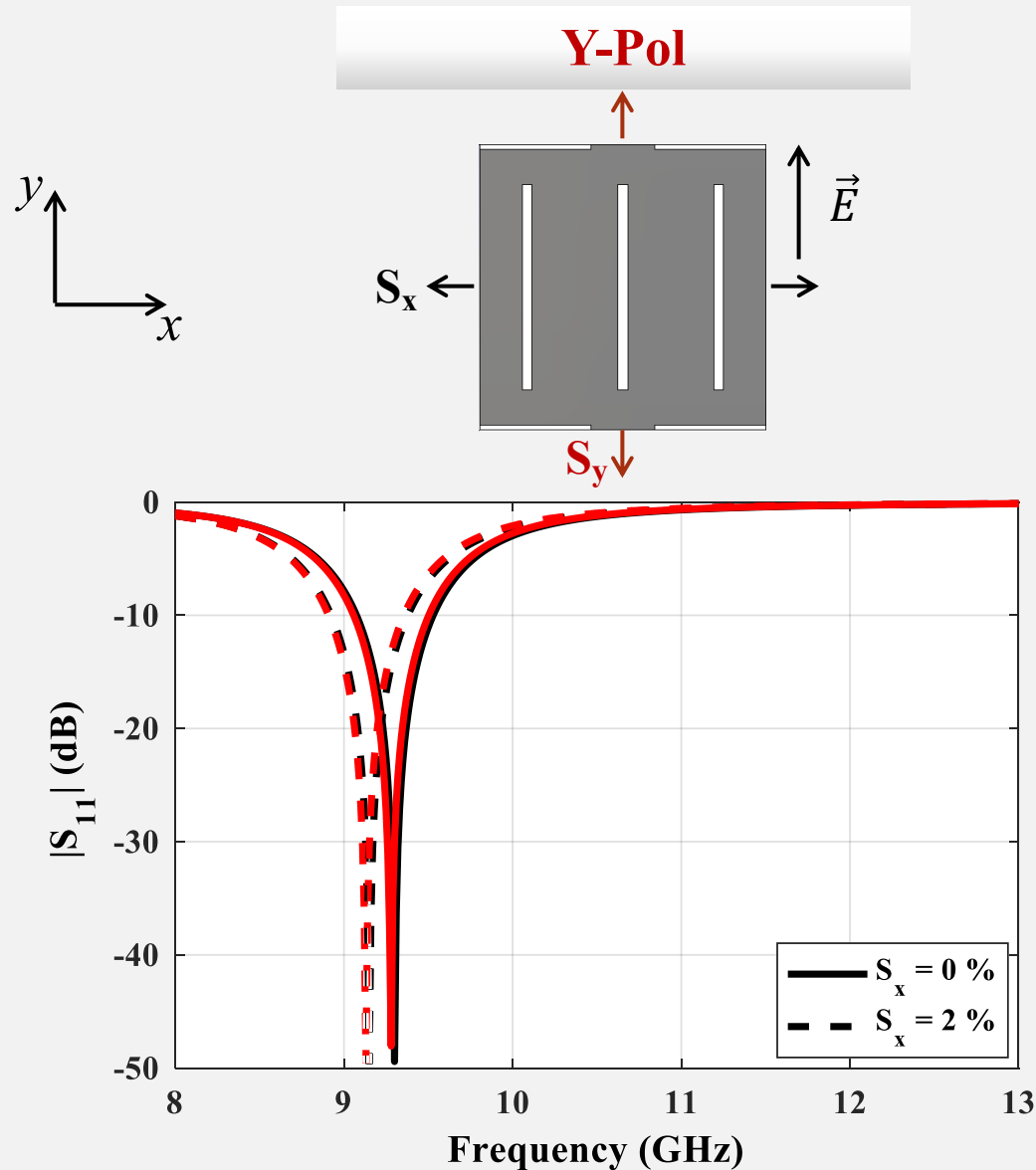
**Y-Pol**

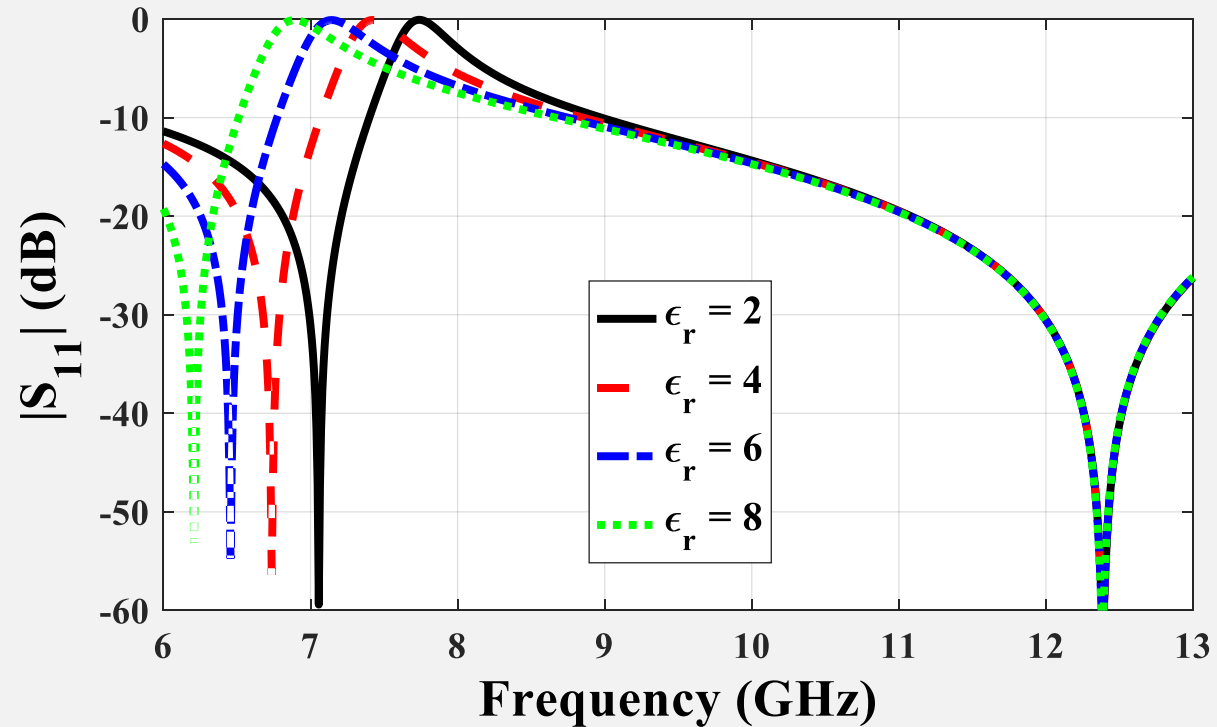
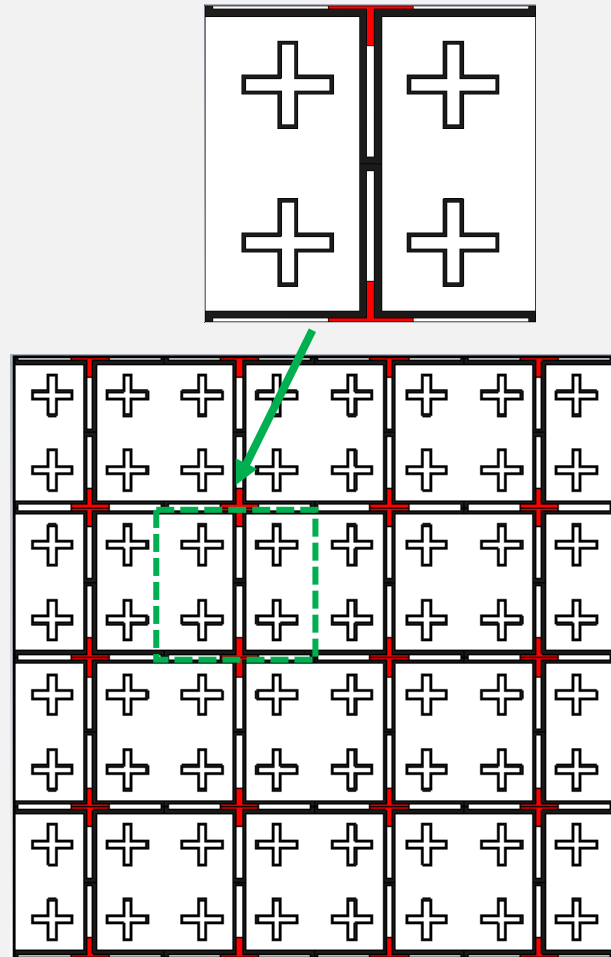


**X-Pol**



# Frequency Response of the Sensor





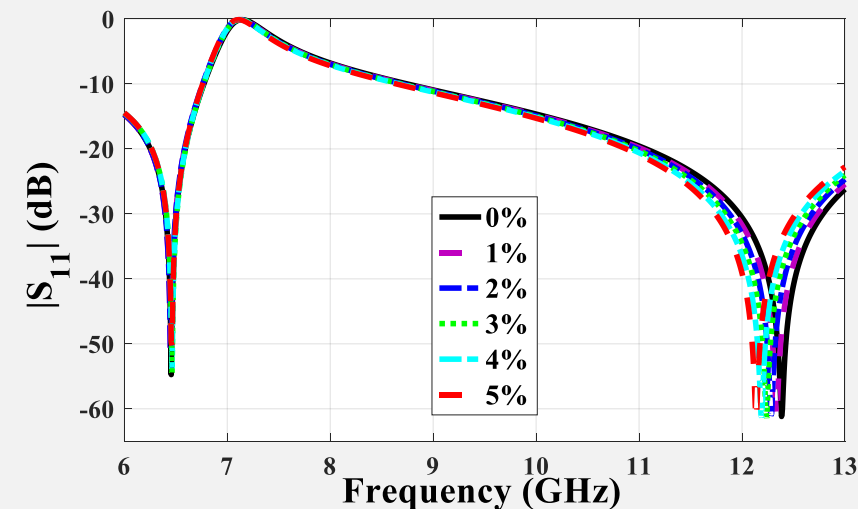
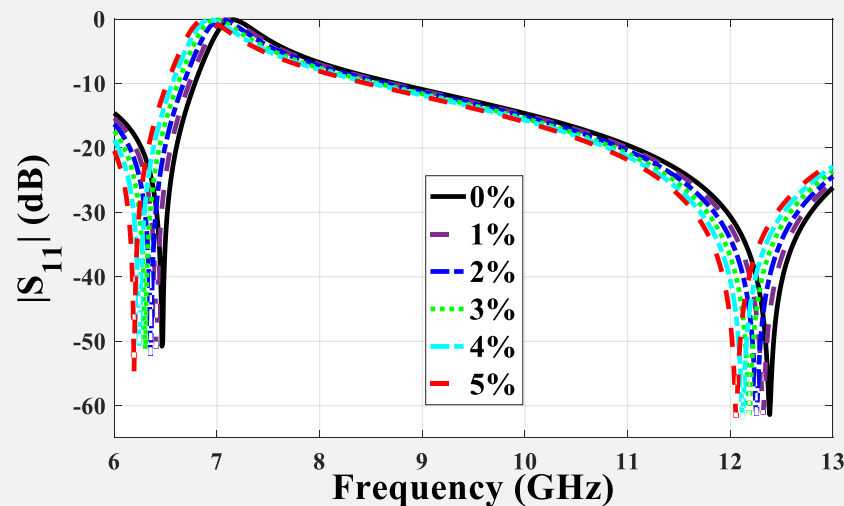
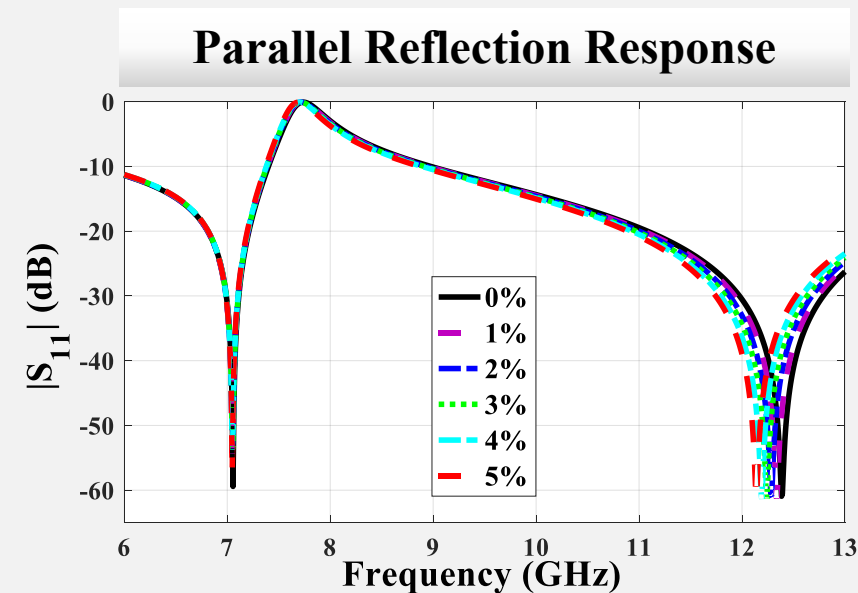
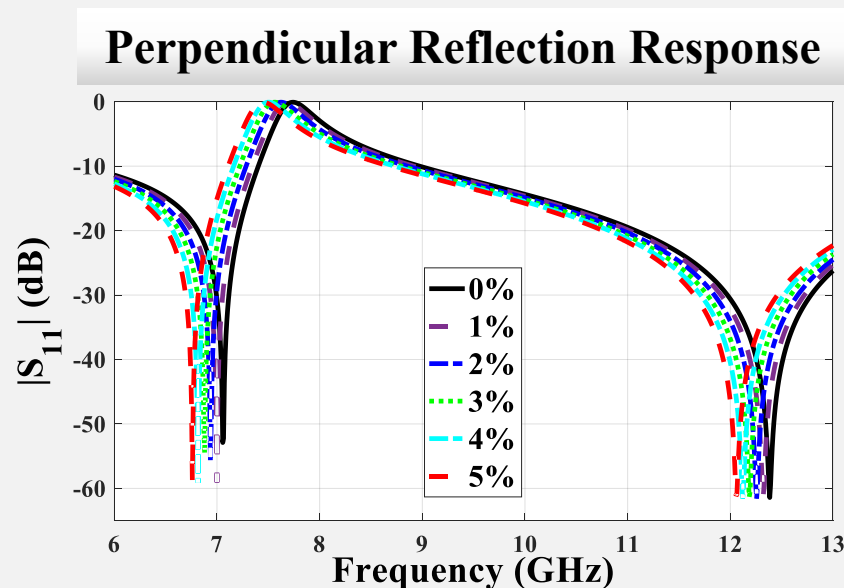
# Concurrent Temperature & Strain Sensing

**Case #1:**

$$\varepsilon_{r1} = 2 \propto T_1$$

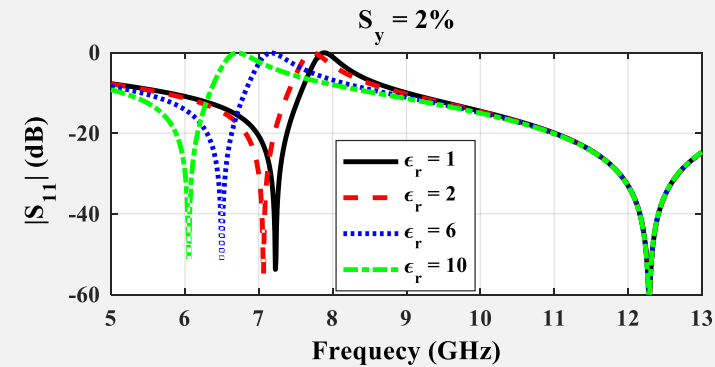
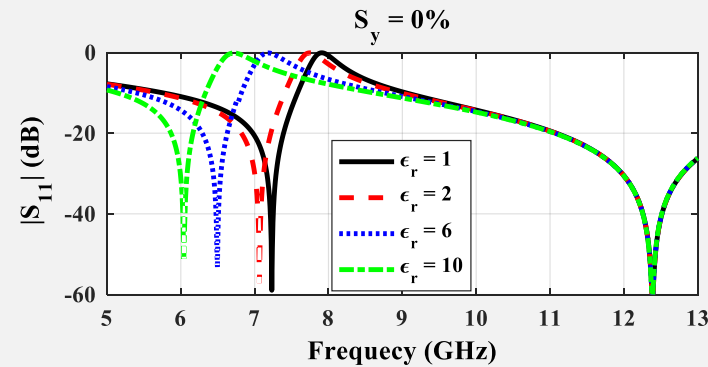
**Case #2:**

$$\varepsilon_{r2} = 6 \propto T_2$$

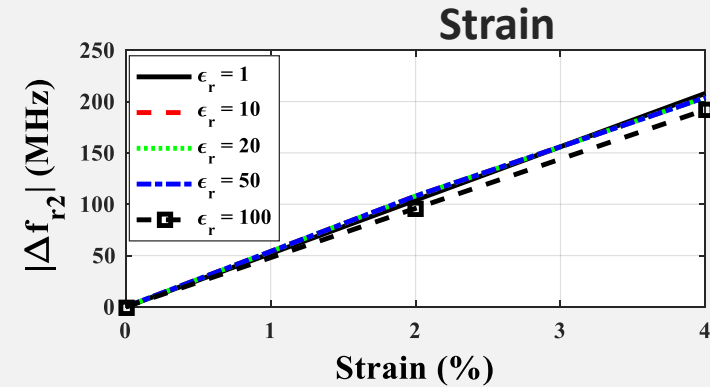
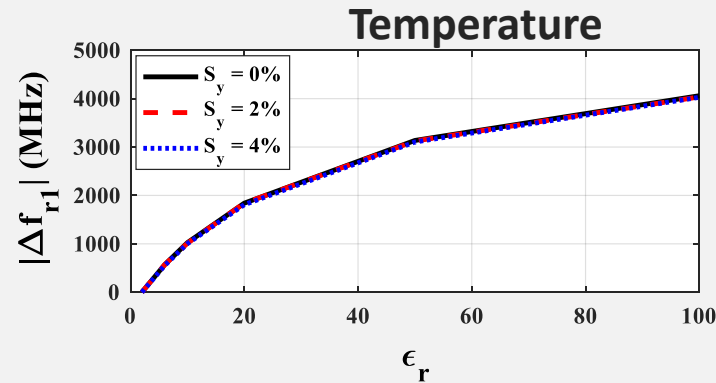


# Simulated Sensor Performance

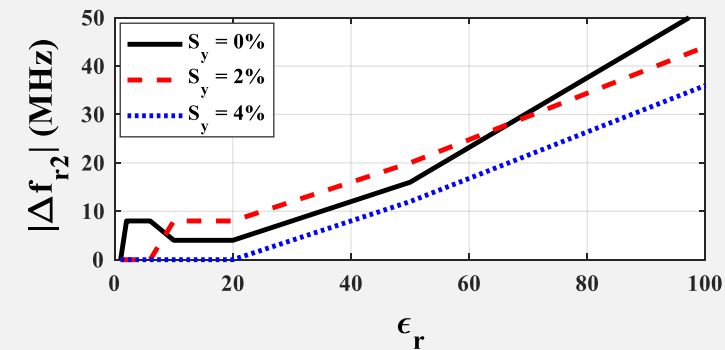
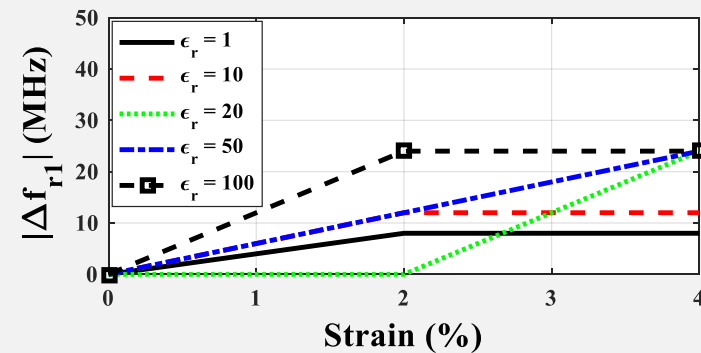
Frequency Response



Sensitivity



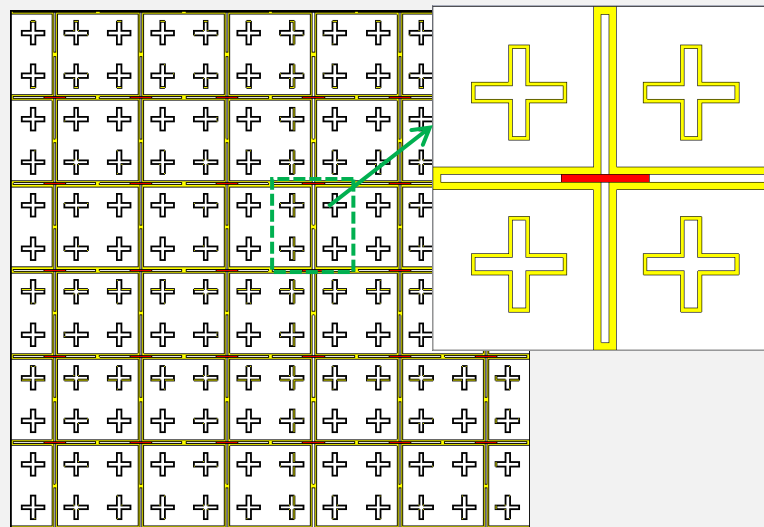
Error



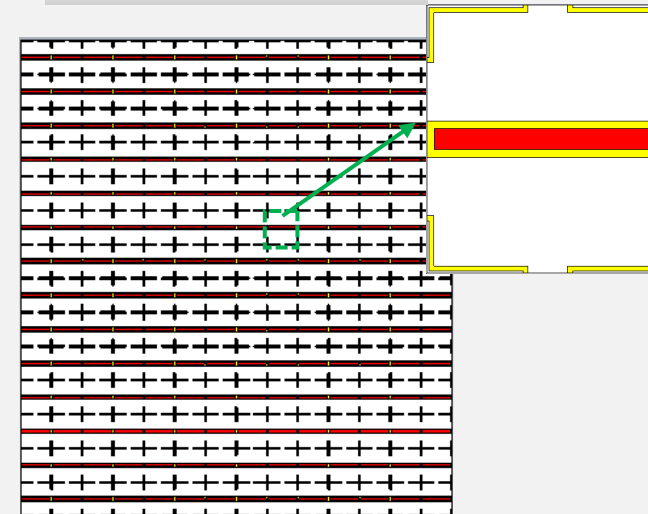


- Upgraded to a grounded FSS in order to remove the effect of background material(s) on the sensor performance.
- Operating frequency band has been increased to Ku-band (12.4 – 18 GHz) to improve resolution.
- Improved sensitivity to temperature.

**X-band Design**

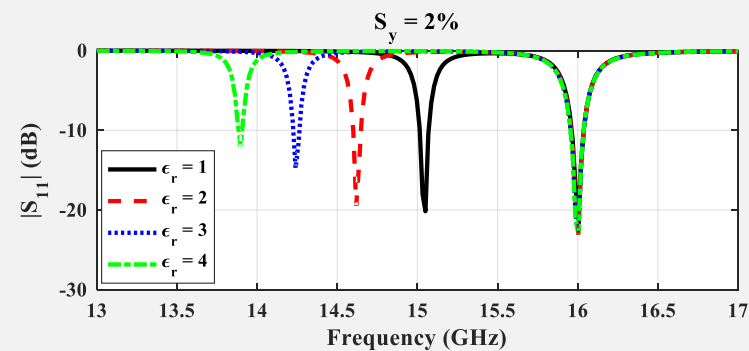
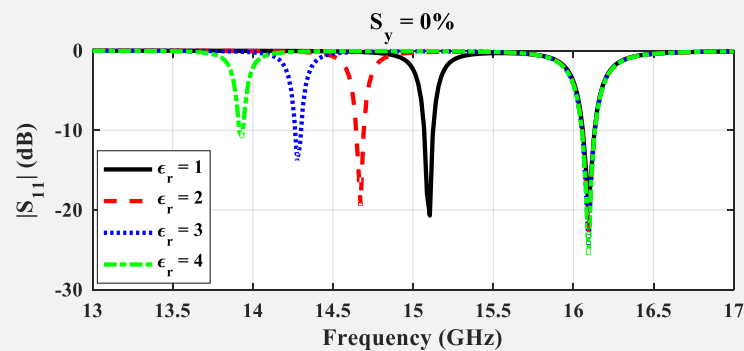


**Ku-band Design**

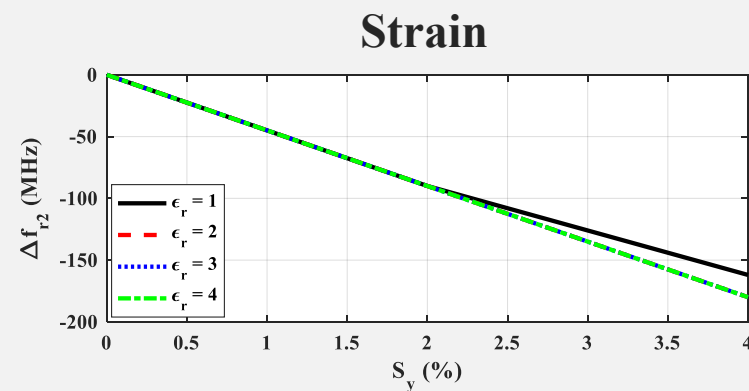
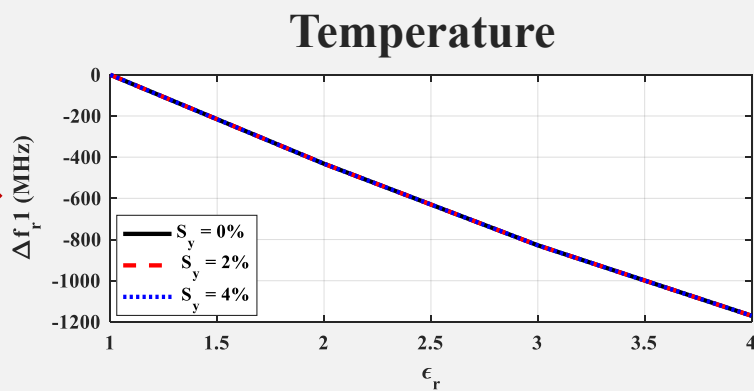


# Simulated Ku-Band Sensor Performance

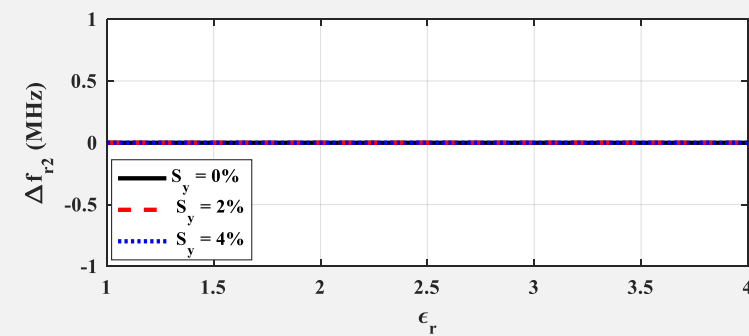
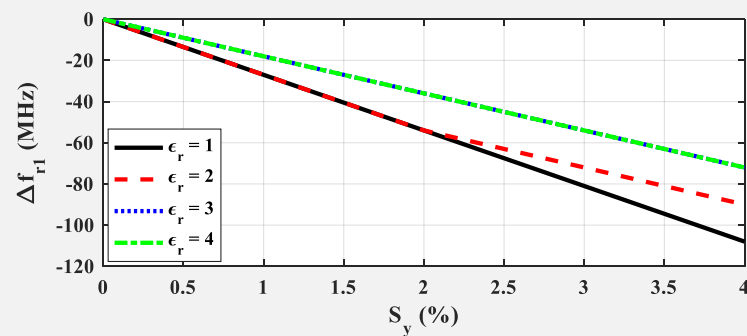
Frequency Response



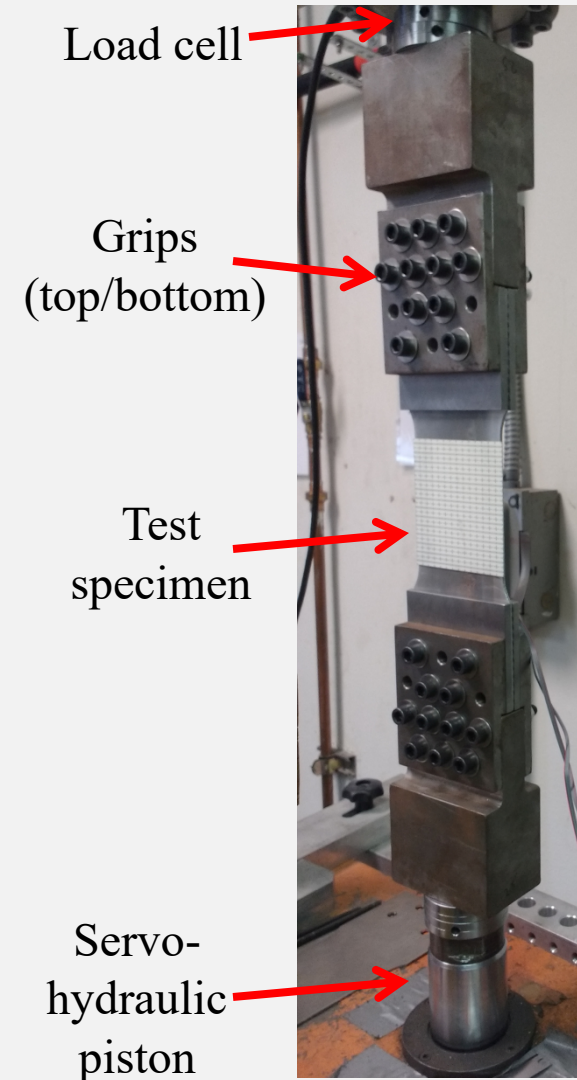
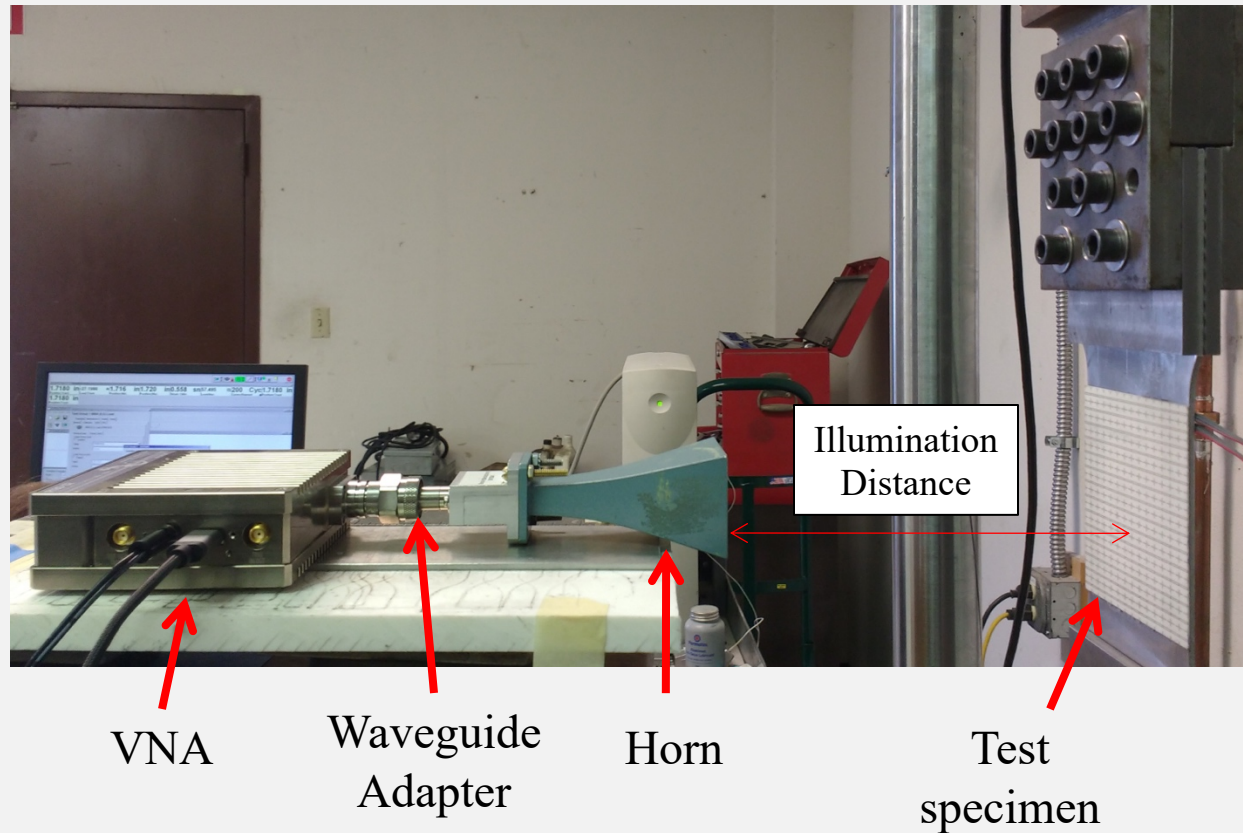
Sensitivity



Error



# Experimental Setup for Strain Measurement

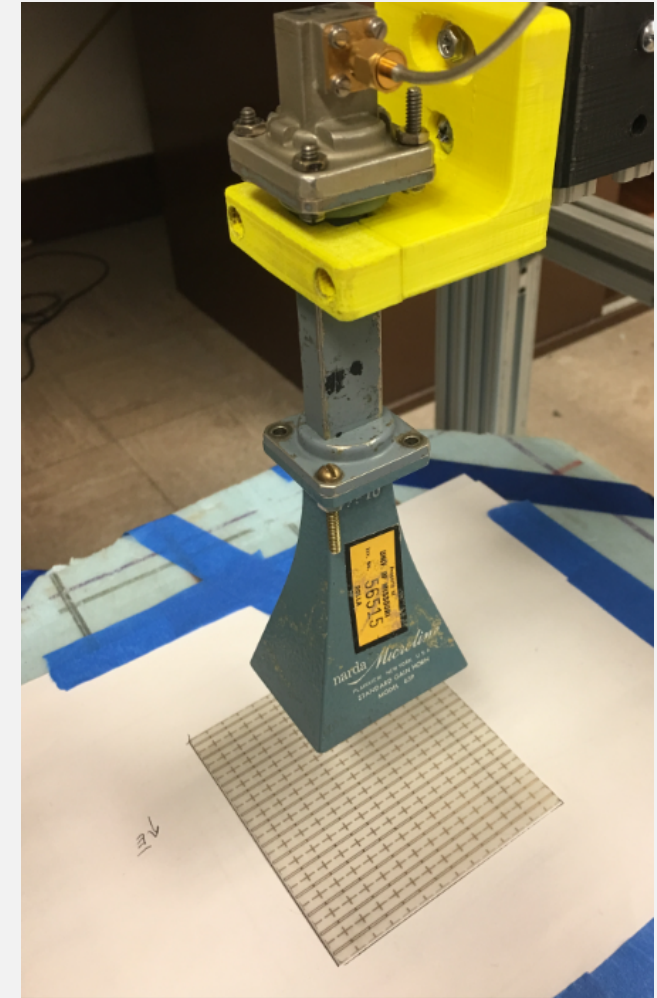
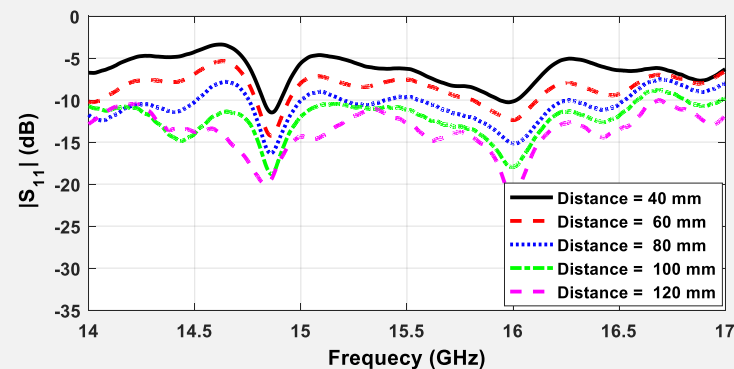
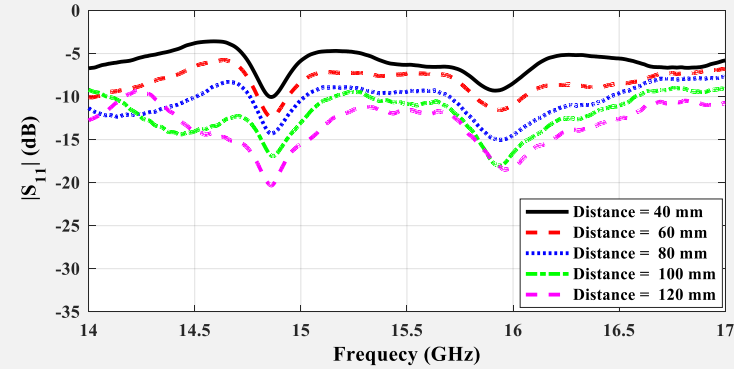
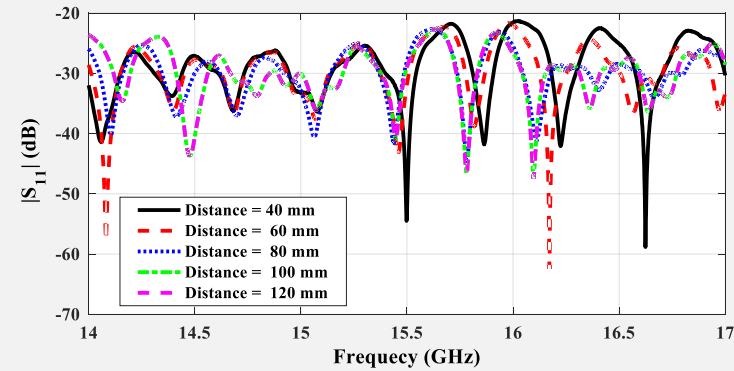


# Measurements Prior to Load Testing

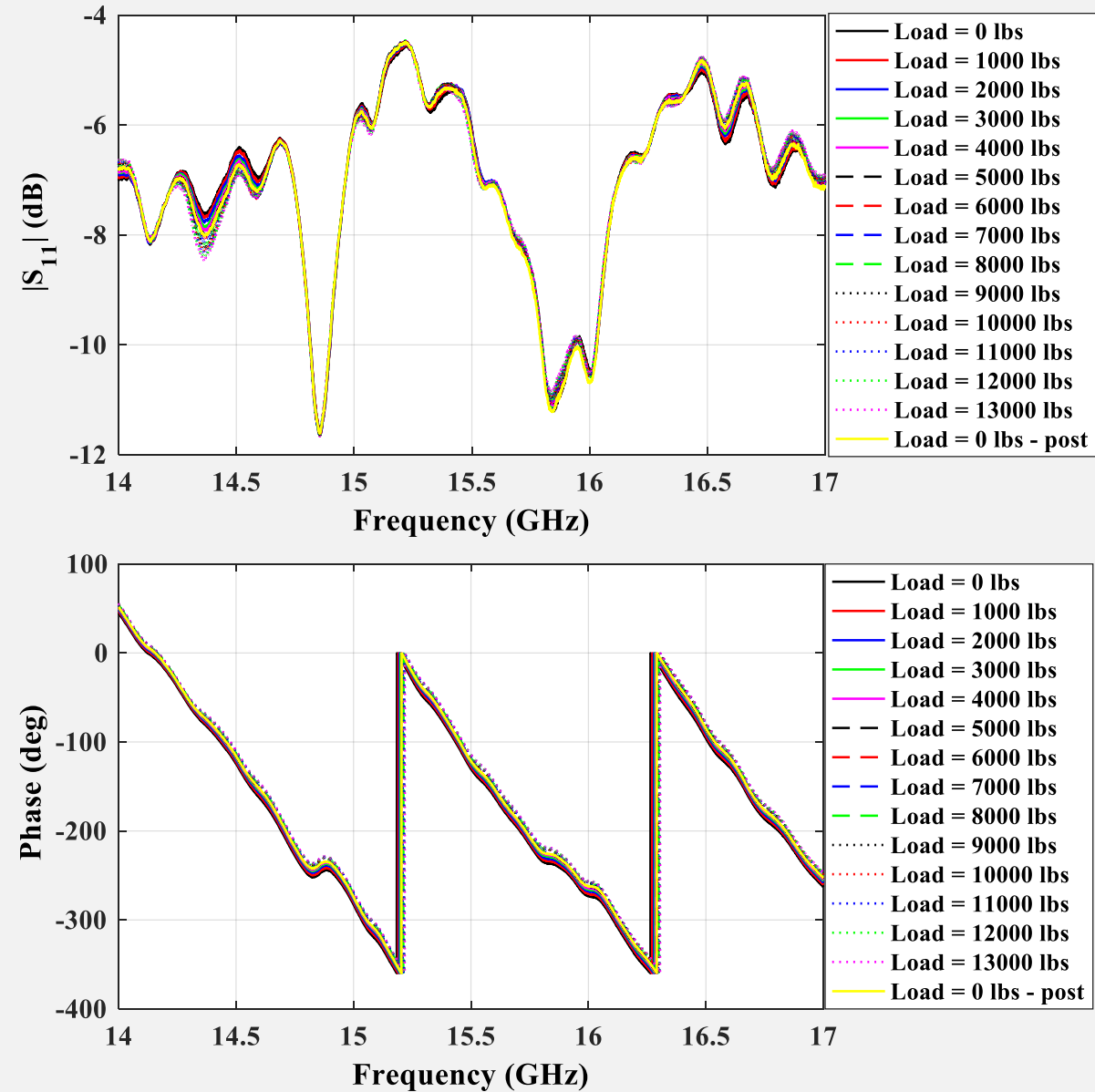
Background

Entire FSS

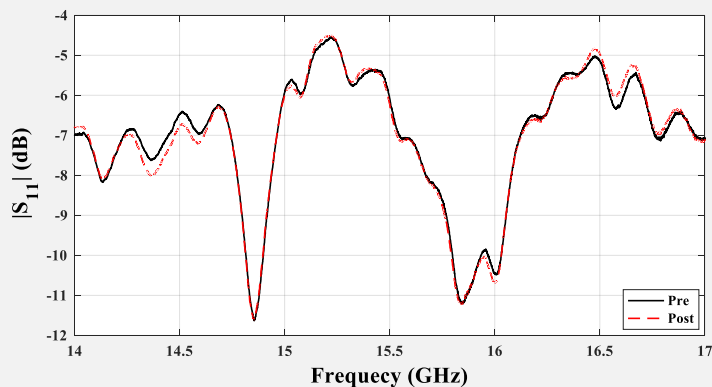
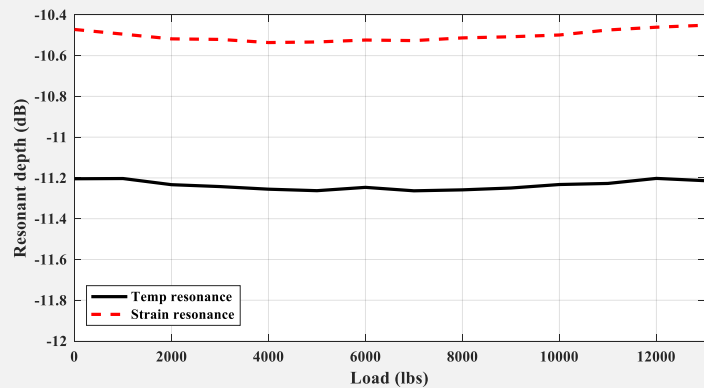
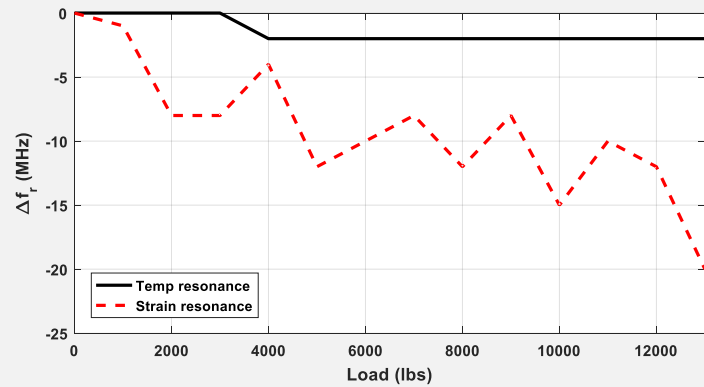
Background Subtracted



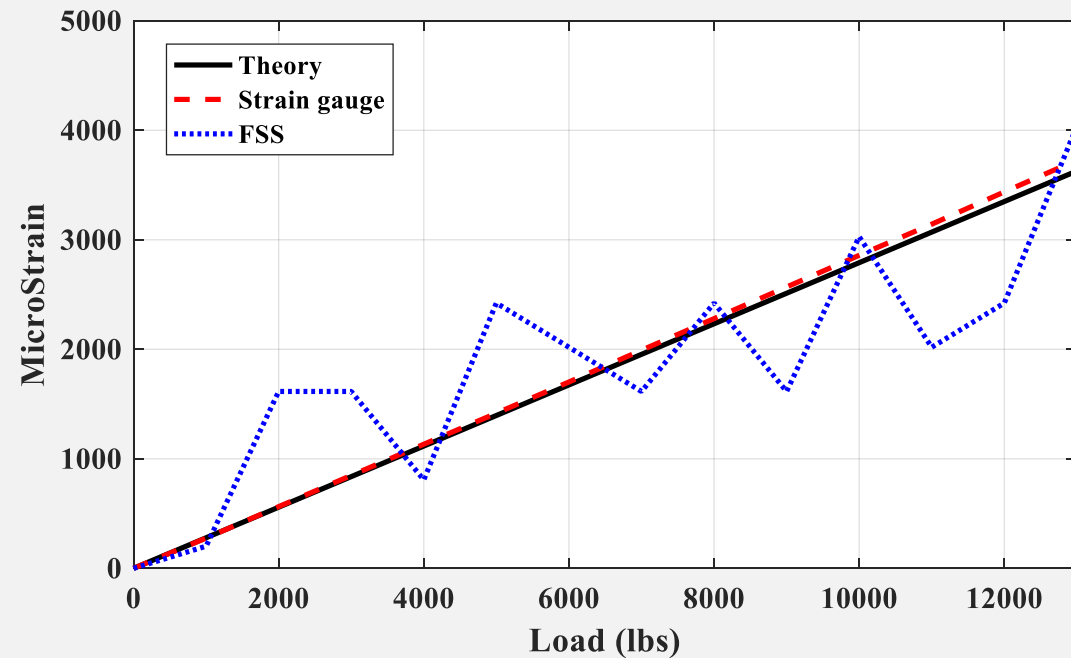
# FSS Measurement Under Load



# FSS Sensor Response Under Load



Calculated strain from frequency shift in (second) strain-sensing resonance vs. strain gauge measurement and theory.

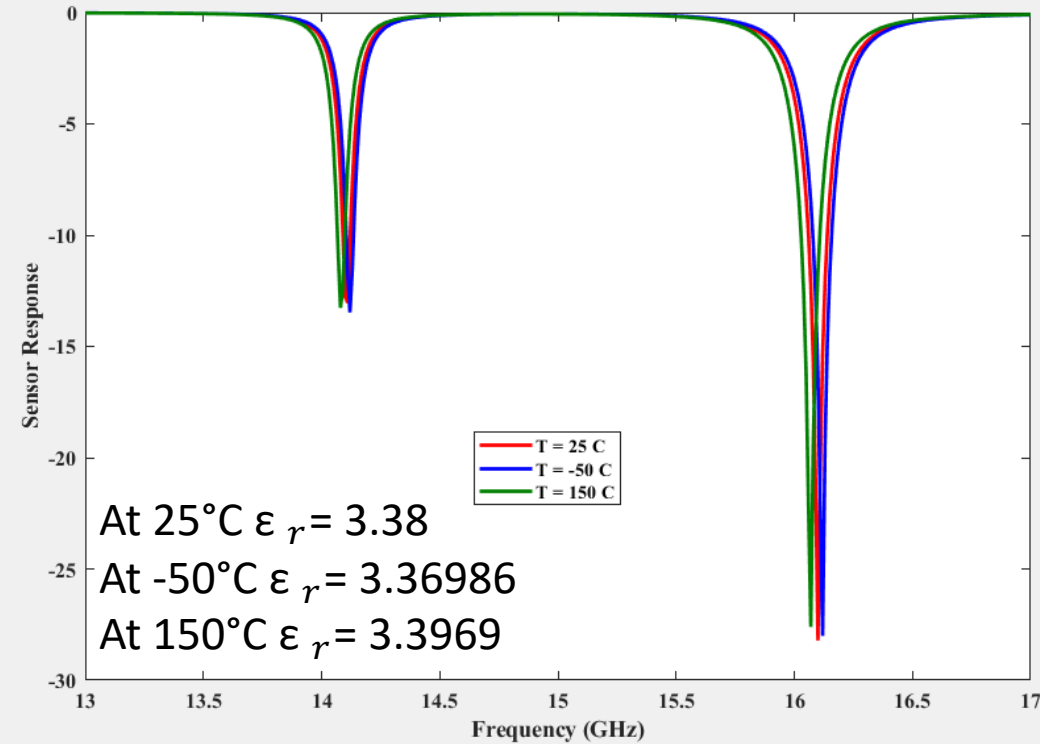
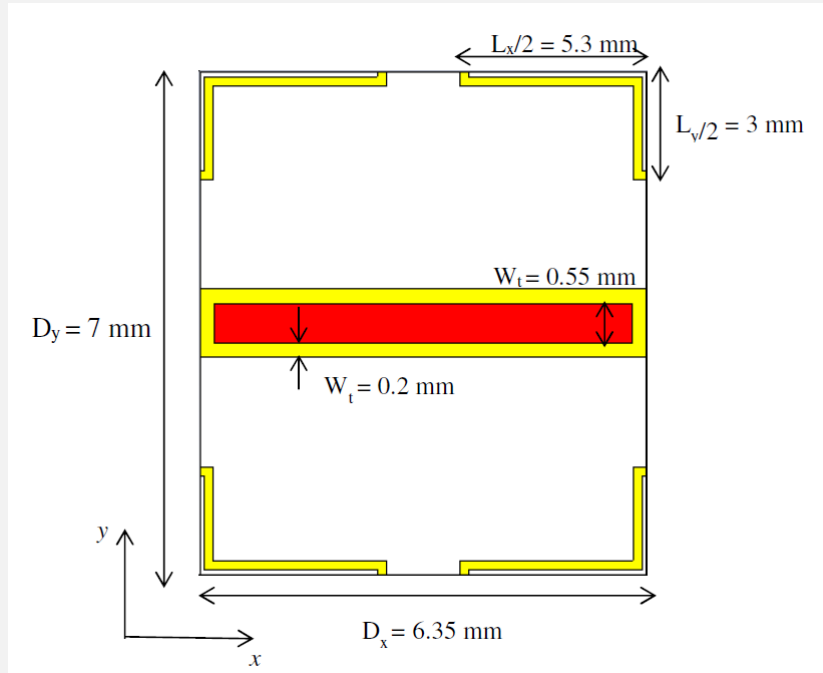




# Other Practical Considerations

- Delamination of the sensor from the test structure is an ongoing concern.
  - Currently investigating adjusting the shape of the sensor to reduce the chances of a lamination failure (particularly at the sensor corners).
- High (extreme) temperature applications will also be challenging due to thermal concerns related to bonding material, temperature-sensitive dielectric, etc.
- Cross sensitivity to other environmental parameters such as humidity, substrate effects (primarily thermal properties), dust contaminants....
- Substrate effects (thermal properties): *temperature dependence of permittivity ( $\epsilon_r$ ) and coefficient of thermal expansion ( $\alpha$ )*

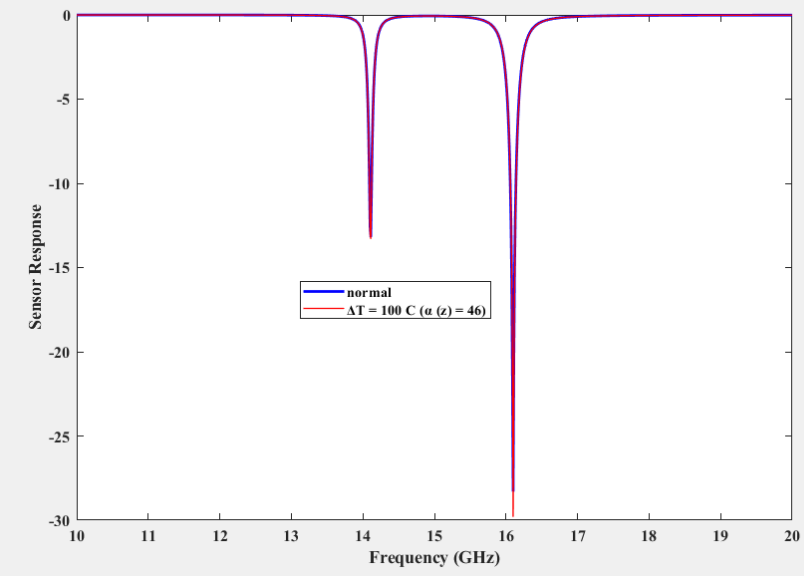
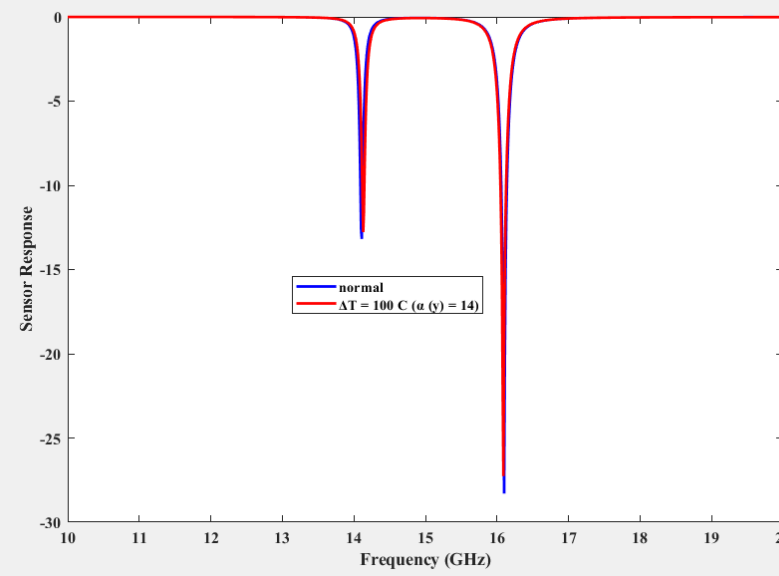
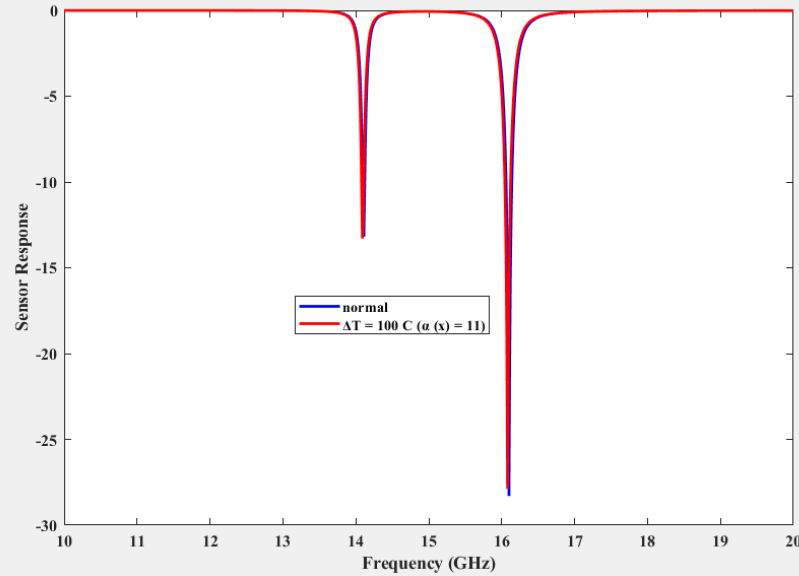
# Temperature Dependence due to $\epsilon_r$



Temperature (°C)	First resonant frequency (GHz)	Frequency Shift (GHz)	Second resonant frequency (GHz)	Frequency Shift (GHz)
25	14.11	-	16.1	-
-50	14.12	0.01	16.12	0.02
150	14.08	-0.03	16.07	-0.03



# Temperature Dependence due to $\alpha$

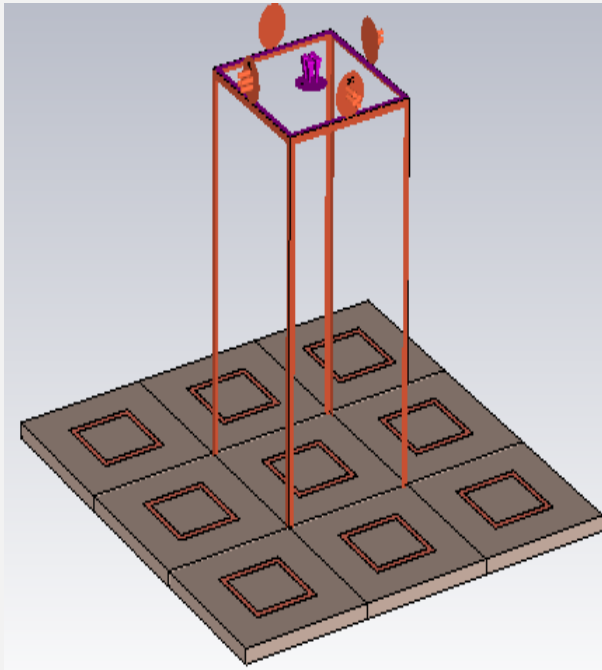


Direction of Length Change	1 <sup>st</sup> Resonant Frequency (GHz)	Frequency Shift (GHz)	2 <sup>nd</sup> Resonant Frequency (GHz)	Frequency Shift (GHz)
Nominal	14.11	-	16.1	-
X	14.09	-0.02	16.08	-0.02
Y	14.13	0.02	16.09	-0.01
Z	14.11	0	16.1	0

# FSS Sensing Challenges - Infinite to Finite

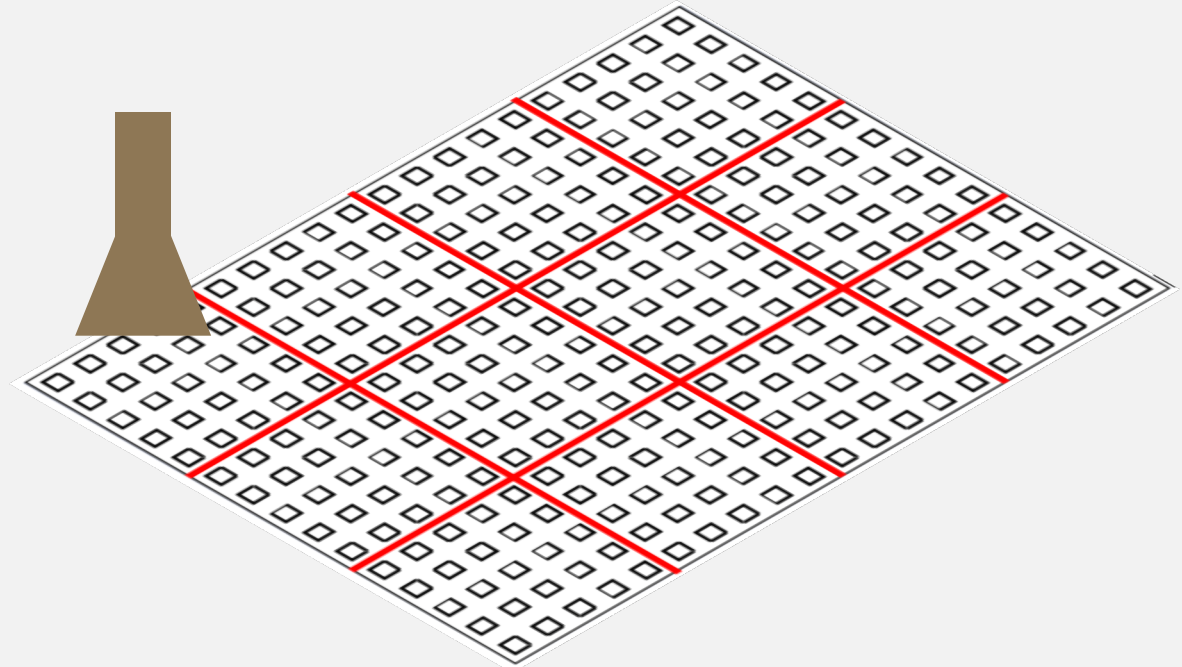
## Infinite FSS

- Infinite array of elements
- Uniform excitation
- Comprehensive frequency response (**low resolution**)



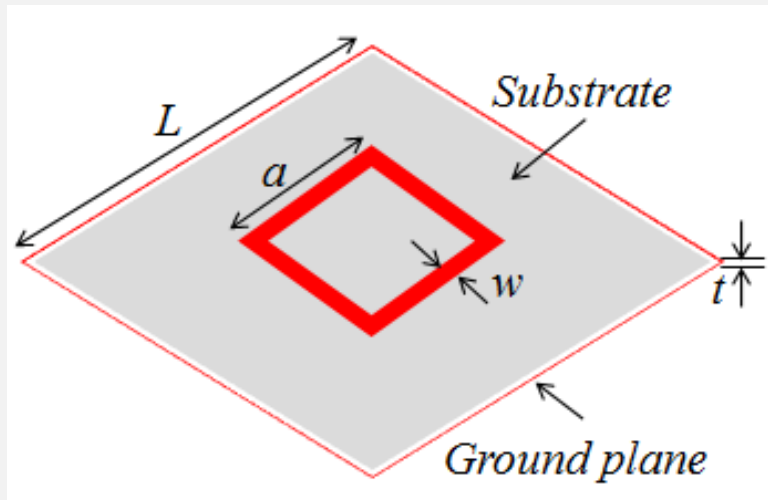
## Finite FSS

- Finite array of elements
- Non-uniform excitation
- Edge effect on frequency response
- Importance of number of unit cells
- Comprehensive vs. localized illumination – resolution!!!



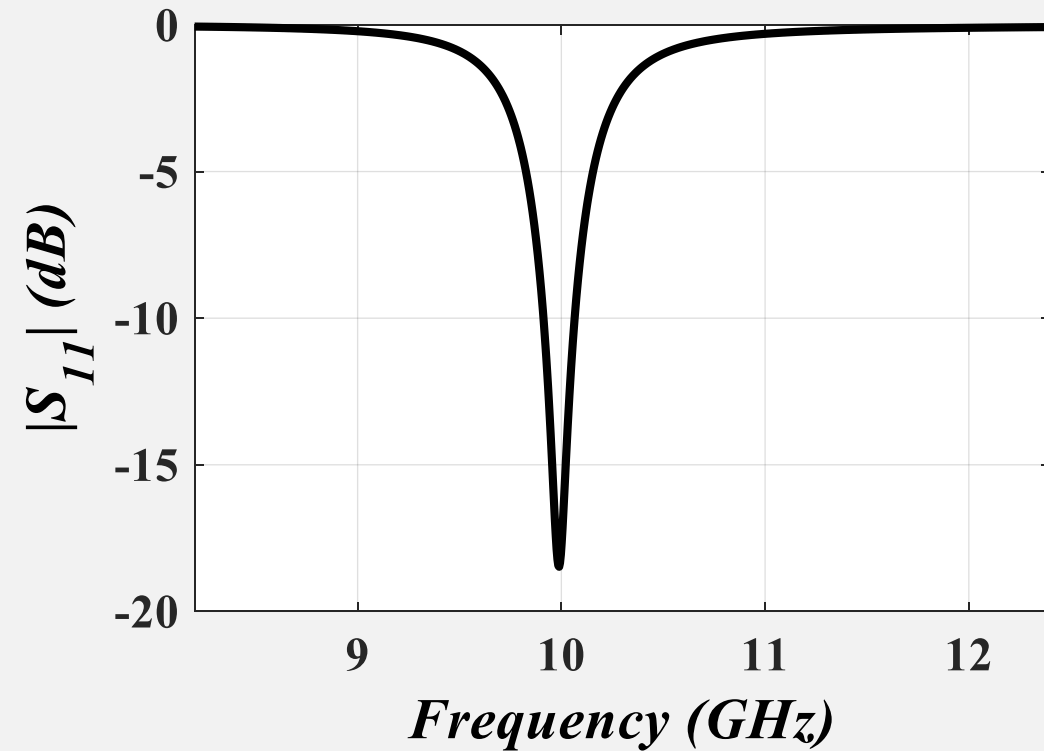
# Ideal FSS Response

Loop unit cell



Substrate: FR-4,  $\epsilon_r = 4.3$ ,  $\tan\delta = 0.023$   
 $L = 10$  mm,  $a = 4.95$  mm,  $w = 0.4$  mm,  $t = 32$  mils

Infinite FSS response



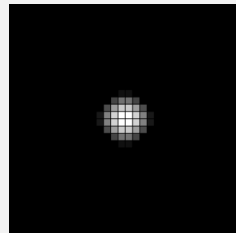
# Sensing Resolution

- Parameters that affect sensor resolution:
  - Illumination footprint (size) on the sensor.
  - Sensor cell size.
  - Number of elements within a sensor cell.

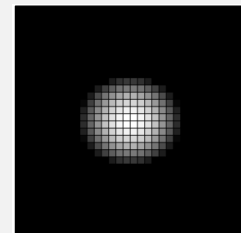
Standoff ( $h$ ):



$2\lambda_0$  (6 cm)



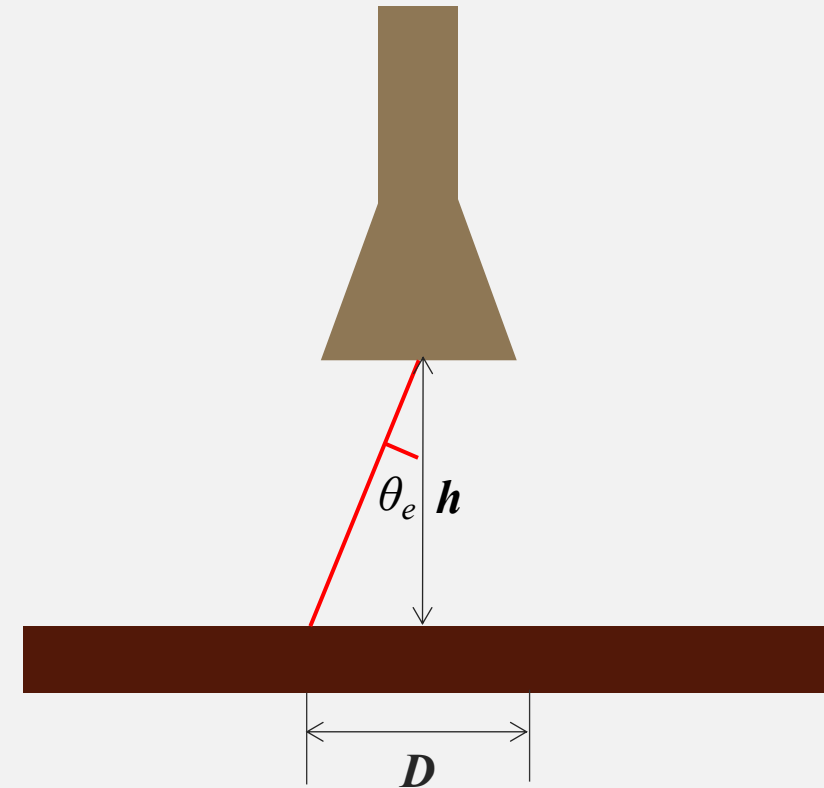
$5\lambda_0$  (15 cm)



20 cm

20 cm

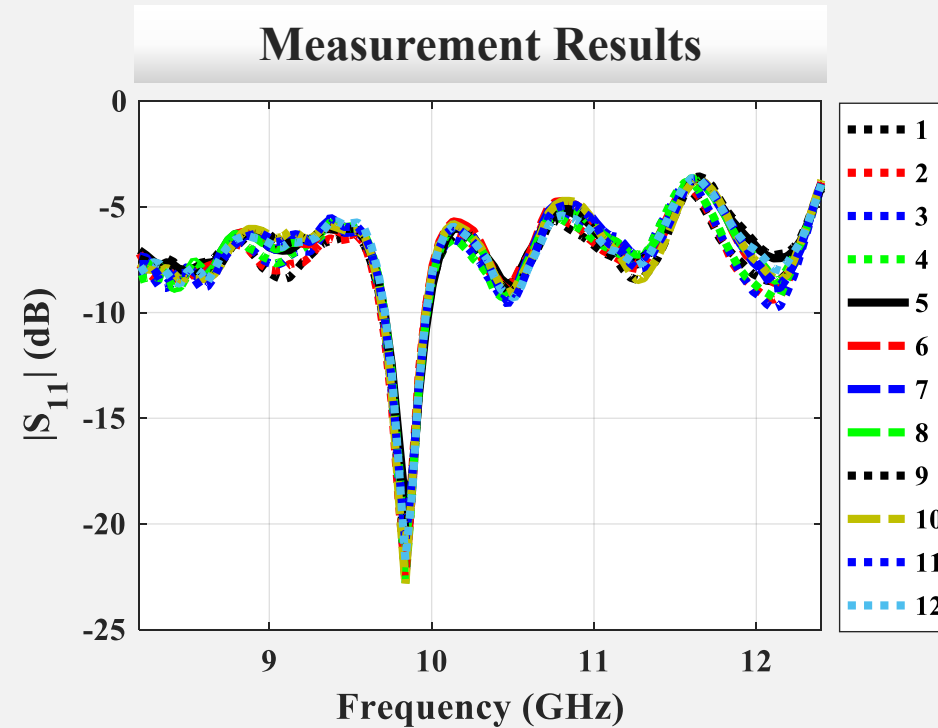
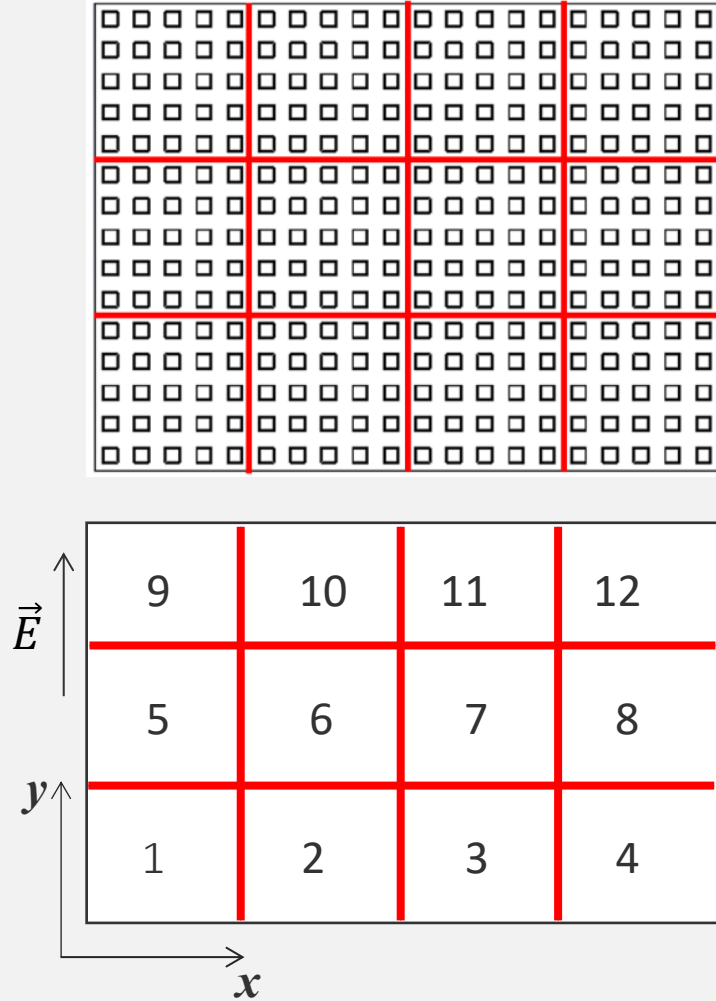
Horn



$$\tan\theta_e = \frac{D}{2h}$$

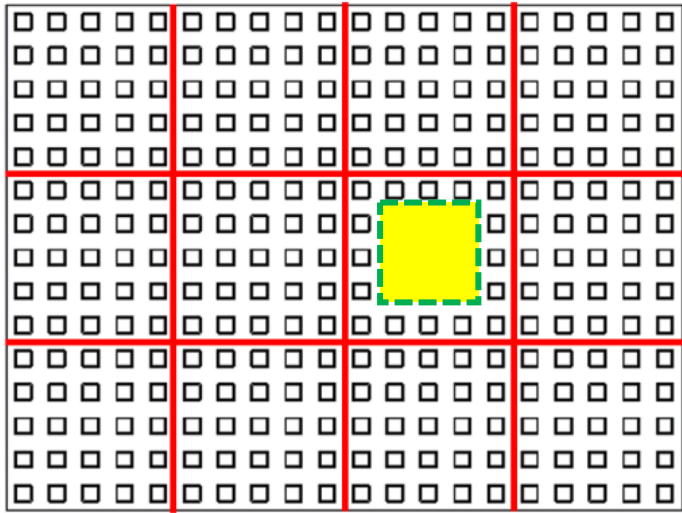
$D$ : sensor cell size;  
 $h$ : illumination distance from sensor.

# Localized Sensing Measurements

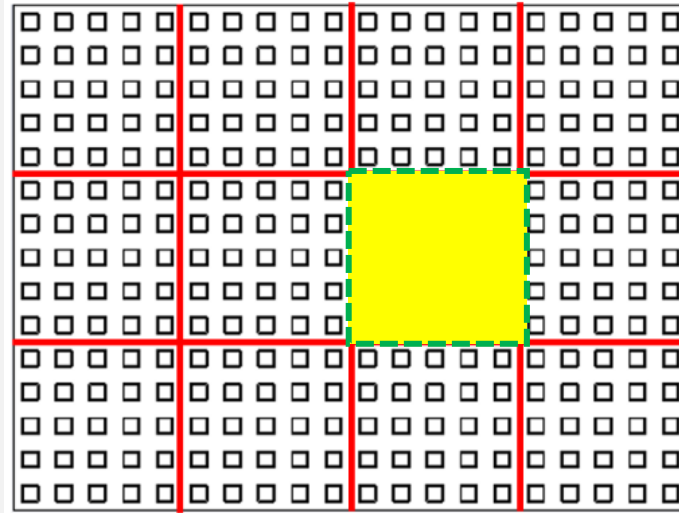


# Localized Sensing – Simulated Strain

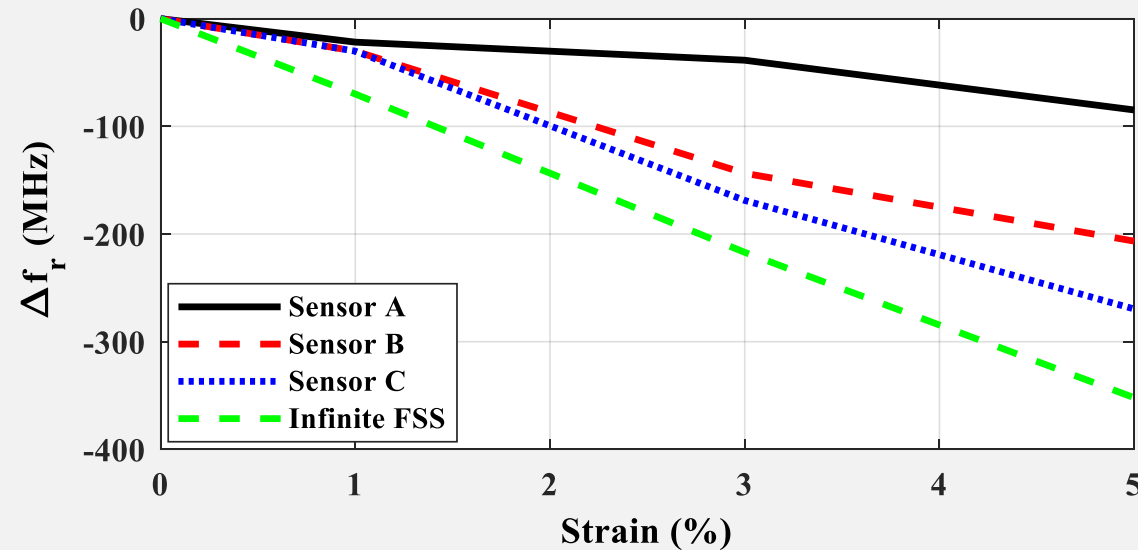
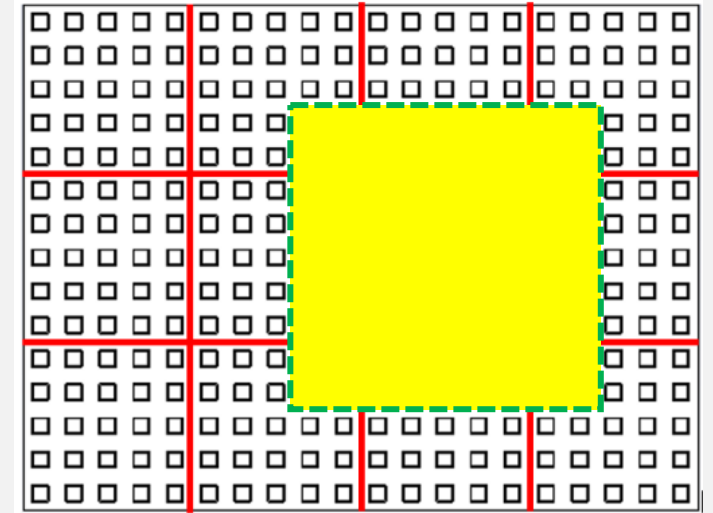
Sensor A



Sensor B

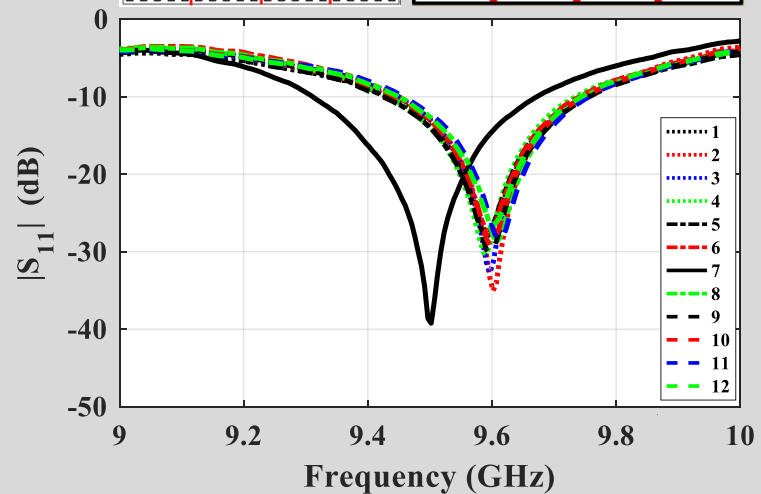
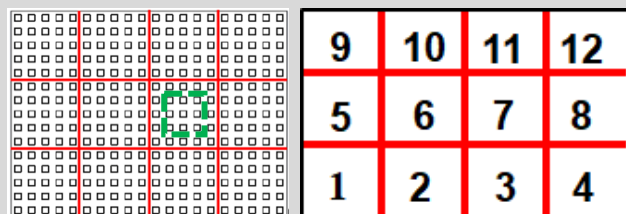
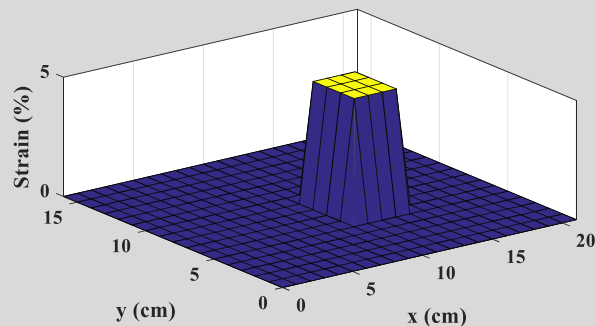


Sensor C

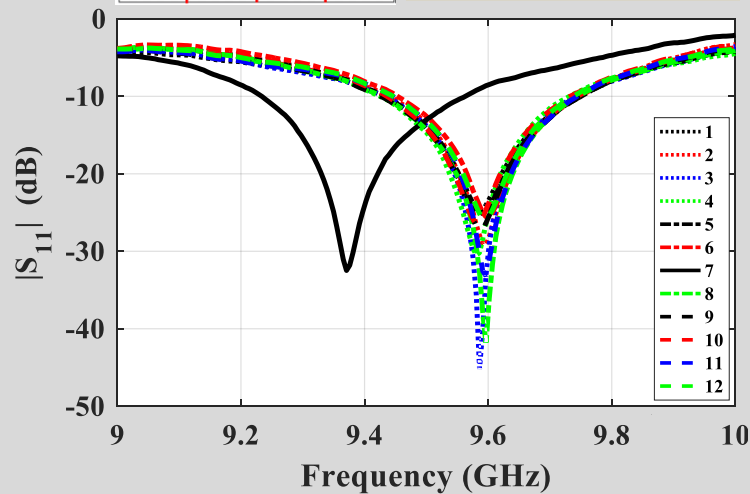
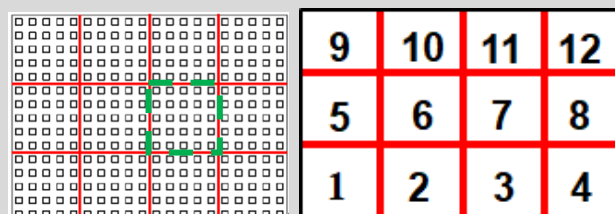
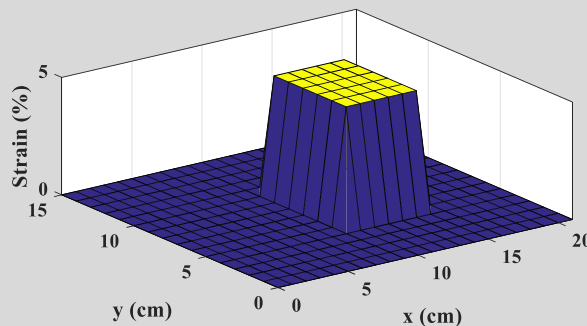


# Localized Sensing - Measurements

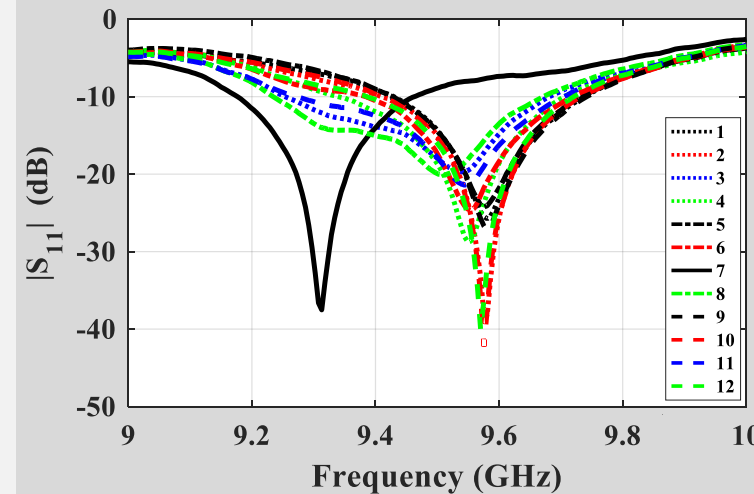
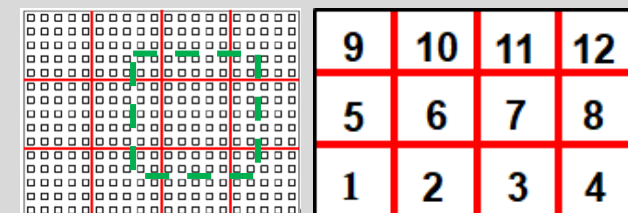
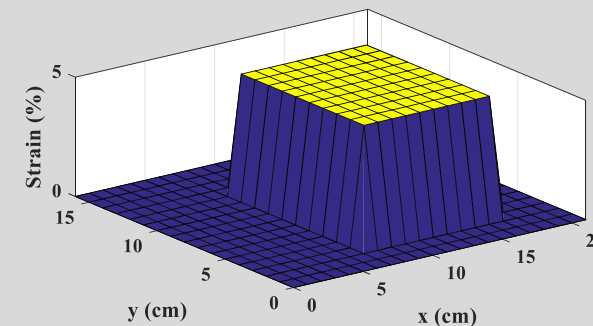
3×3 Elements  
Strained area < Sensor cell area



5×5 Elements  
Strained area = Sensor cell area

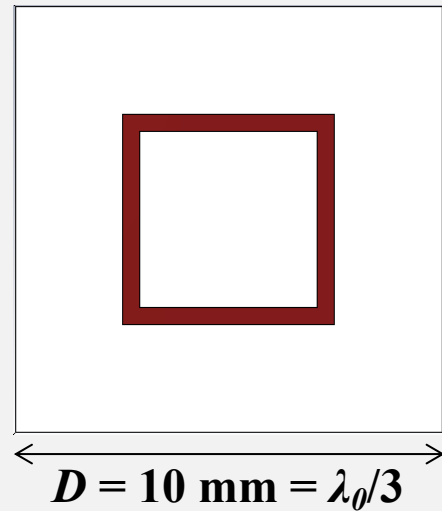


9×9 Elements  
Strained area > Sensor cell area



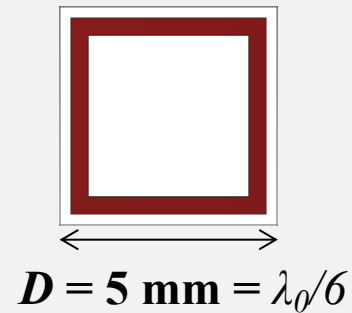
# Sensor Improvement by Miniaturization

Original FSS



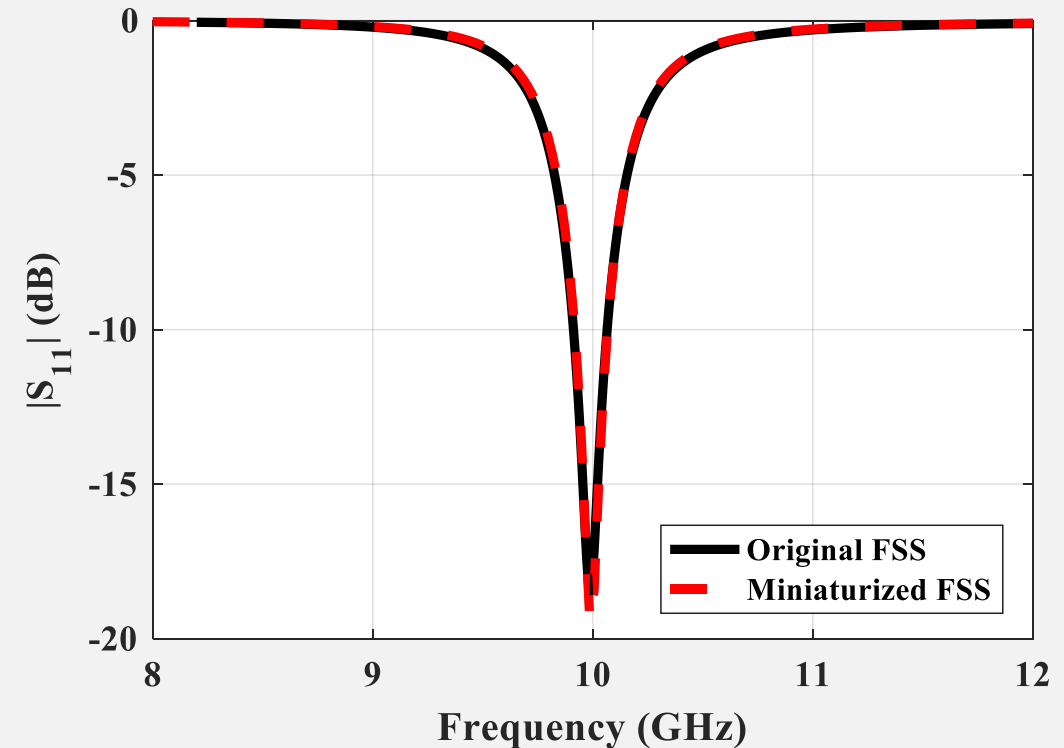
FR-4 Substrate:  $t = 32 \text{ mils}$

Miniaturized FSS



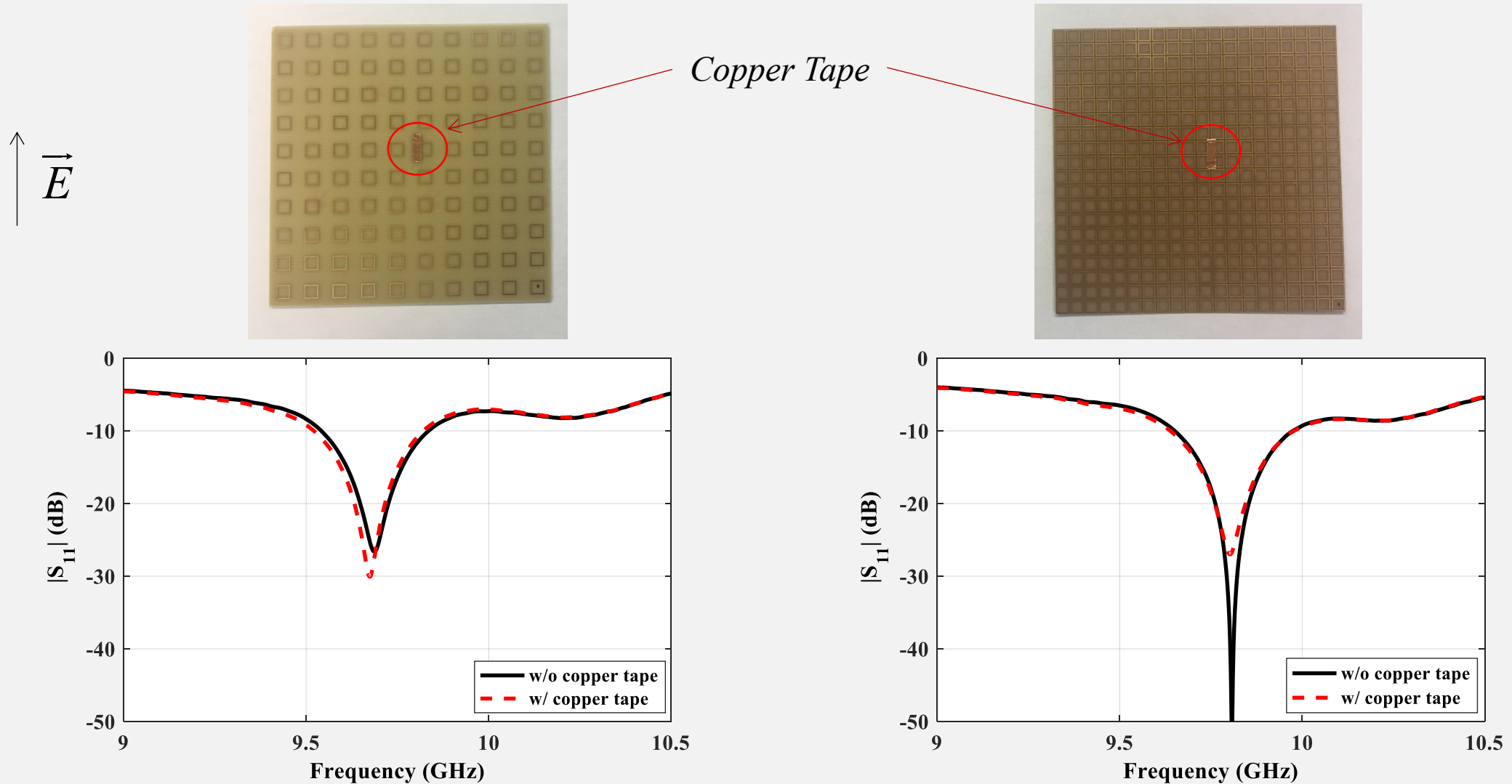
$t = 15 \text{ mils}$

Ideal FSS Response (Simulation)





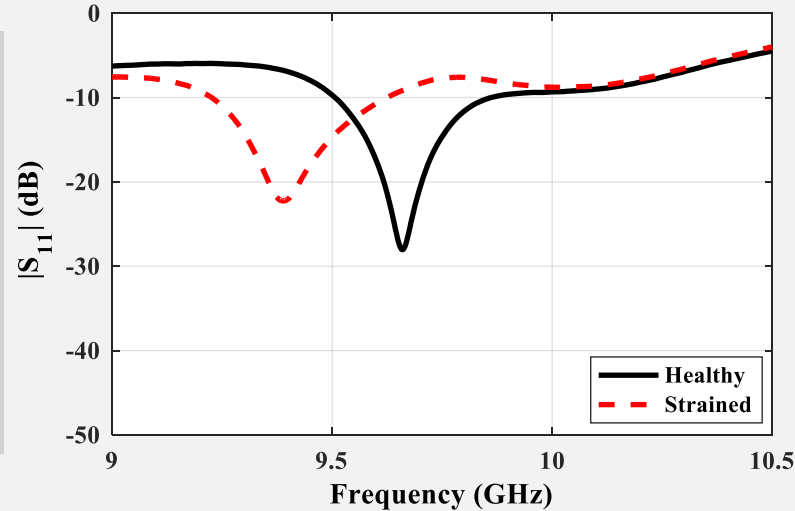
# Effect of Anomaly on the Sensor Response



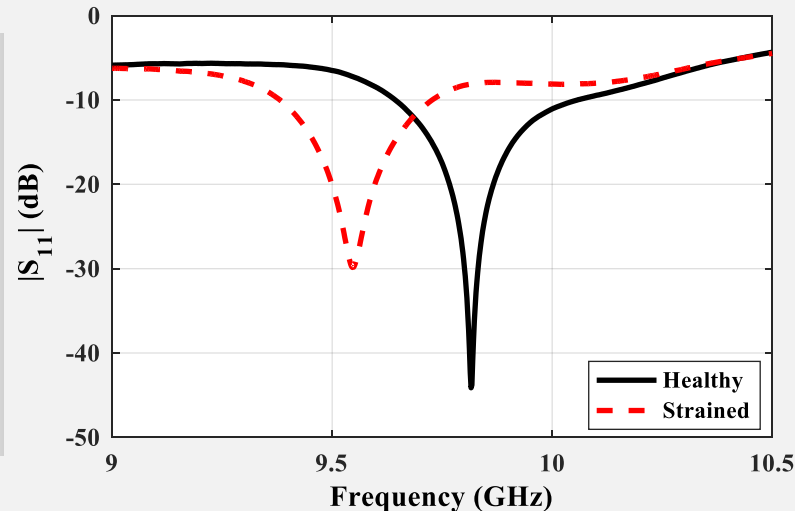
# Practical Example – Sensor Miniaturization

- Effect of strain is modeled by increasing sensor dimensions by 5% in strained direction.
- Interrogating polarization is parallel to direction of strain.
- Similar frequency shift since element dimensions of both sensors are similar.

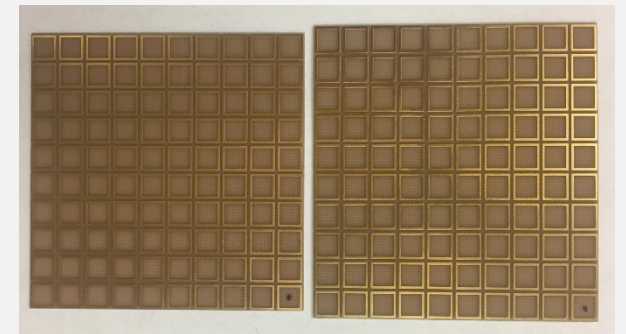
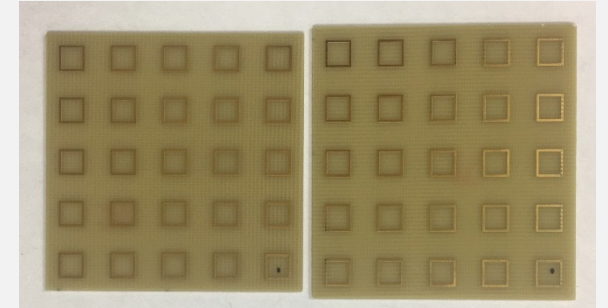
Original FSS



Miniaturized FSS



unstrained      strained



# Concluding Remarks

- FSS-based sensors have strong potential as a solution for numerous sensing needs
  - Wireless interrogation and flexible resolution provides unique capabilities
- Extreme design flexibility
- Highlighted a number of successful applications including multi-parameter (temperature and strain) sensing
- Some practical challenges remain, but the future for FSS-based sensing continues to progress and expand.....

# Acknowledgment

- This work was primarily supported by a National Aeronautics and Space Administration STTR Phase I (T12.01 Advanced Structural Health Monitoring) award (Contract #NNX17CL92P).

# Thank You



Any Questions?